# CSR Calculation in Paraxial Approximation

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# Derivation

- Geometry
  - Use (x,y,s) coordinate
    (to make the source trajectory on grid)
  - Bending in x-plane

$$d\mathbf{r} = g(x,s)\mathbf{e}_s ds + \mathbf{e}_x dx + \mathbf{e}_y dy,$$

$$g(x,s) = 1 + \frac{x}{\rho(s)}$$

- Approximation
  - Ignore d<sup>2</sup>/ds<sup>2</sup> (paraxial approx.)
  - Other approx.
    - $\gamma \rightarrow \text{infinite}$
    - a : typical aperture

$$\epsilon \equiv \sqrt{\frac{a}{\rho}} \ll \mathbf{1}$$

• Transverse component of Maxwell equation

$$\nabla(\nabla \cdot \boldsymbol{E}) - \nabla \times (\nabla \times \boldsymbol{E}) - \frac{\partial^2}{\partial t^2} \boldsymbol{E} = \nabla \rho_e + \frac{\partial \boldsymbol{J}}{\partial t}$$

#### becomes

 $\frac{\partial}{\partial x} \left( \frac{1}{g} \frac{\partial (gE_x)}{\partial x} \right) + \frac{\partial^2 E_x}{\partial y^2} + \frac{1}{g} \frac{\partial}{\partial s} \left( \frac{1}{g} \frac{\partial E_x}{\partial s} \right) - \frac{\partial^2}{\partial t^2} E_x + \frac{2}{\rho g^2} \frac{\partial E_s}{\partial s} - \frac{E_s}{g} \frac{\partial}{\partial s} \left( \frac{1}{\rho g} \right) = \frac{\partial \rho_e}{\partial x} + \frac{\partial}{\partial t} J_x$  $\frac{1}{g} \frac{\partial}{\partial x} \left( g \frac{\partial E_y}{\partial x} \right) + \frac{\partial^2 E_y}{\partial y^2} + \frac{1}{g} \frac{\partial}{\partial s} \left( \frac{1}{g} \frac{\partial E_y}{\partial s} \right) - \frac{\partial^2}{\partial t^2} E_y = \frac{\partial \rho_e}{\partial y} + \frac{\partial}{\partial t} J_y$ 

• Ignoring some small terms in  $\boldsymbol{\epsilon}$  and assuming

$$m{E} \propto e^{-ik(t-s)}$$

$$2ik\frac{\partial E_x}{\partial s} + \Delta_{\perp}E_x + \frac{2k^2x}{\rho}E_x = \frac{\partial\rho_e}{\partial x} - ikZ_0J_x - \frac{\partial^2 E_x}{\partial s^2} + x\left(\frac{\partial}{\partial s}\frac{1}{\rho}\right)\frac{\partial E_x}{\partial s} + \left(\frac{\partial}{\partial s}\frac{1}{\rho}\right)E_s - \frac{2\partial E_s}{\partial s}$$
$$2ik\frac{\partial E_y}{\partial s} + \Delta_{\perp}E_y + \frac{2k^2x}{\rho}E_y = \frac{\partial\rho_e}{\partial y} - ikZ_0J_y - \frac{\partial^2 E_y}{\partial s^2} - \frac{1}{g}\frac{\partial g}{\partial s}\left(ikE_y + \frac{\partial E_y}{\partial s}\right)$$

• Terms on the r.h.s. are small except

$$x\left(\frac{\partial}{\partial s}\frac{1}{\rho}\right)\frac{\partial E_x}{\partial s}$$

- This causes delta function at magnet edges
- For finite edge length, the jump of E<sub>x</sub> is

$$\delta E_x \sim \frac{\epsilon^2}{k \cdot l_{edge}} E_x, \qquad (l_{edge} = edge \ length)$$

- This term can be ignored if the bunch length is comparable or shorter than the edge length
- One this term is ignored, other terms are smooth and does not cause problem with hard edge magnet

• Ignoring second derivative in s (paraxial approx) we get

$$\frac{\partial}{\partial s} \begin{pmatrix} E_x \\ E_y \end{pmatrix} = \frac{i}{2k} \left[ \left( \Delta_{\perp} + \frac{2k^2 x}{\rho} \right) \begin{pmatrix} E_x \\ E_y \end{pmatrix} - Z_0 \begin{pmatrix} \partial \rho_e / \partial x \\ \partial \rho_e / \partial y \end{pmatrix} \right]$$

• Longitudinal field can be calculated by

$$E_s = \frac{i}{k} \left( \frac{\partial E_x}{\partial x} + \frac{\partial E_y}{\partial y} \right) - \frac{i}{k} Z_0 J_s$$

## Integral in infinite exit pipe

• In the exit pipe  $(E_x, E_y)$  satisfies

$$\frac{dF}{ds} = \frac{i}{2k}MF, \qquad M = \Delta_{\perp}$$

• This can be solved as

$$F(s) = \exp\left(\frac{i}{2k}M(s - s_{exit})\right)F(s_{exit})$$
$$\int_{s_{exit}}^{\infty} F(s)ds = 2ikM^{-1}F(0)$$

- Actually, M<sup>-1</sup> is not needed (solve linear equation)
- Integral of E<sub>s</sub> can be calculated from this integral using the relation between (E<sub>x</sub>,E<sub>y</sub>) and E<sub>s</sub>

# Advantages of Paraxial Approx

- Mesh size can be independent of the wavelength 1/k
- Can be solved as an initial value problem in s
  - Oppositely traveling wave ignored → information one way
  - Only (Ex,Ey) is needed at entrance (no derivatives needed)
  - Analytic treatment also easier
- Can easily include resistive wall effect

# Agreement with Theories

- Agree with Derbenev-Shiltsev formula in vacuum (simulation and analytically)
- Agree with Saldin et.al. for finite length magnet (simulation)
- Agree with Warnock's formula for infinite parallel plates (analytically)
- Agreement of troidal chamber formula has not checked yet (→ Agoh)

# What has not been successful

- Method to calculate the transverse wake
  It seems more careful treatment near the charge is needed
- Going back to the time domain and solve it by mesh