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# **Design and Operation Experience of PLS-II Vacuum System**

2015.01.25

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On behalf of Vacuum Group  
Pohang Accelerator Laboratory

- Brief description of PLS-II
- Design of PLS-II vacuum system
  - Tight space (20 IDs / 280 m)
  - High mechanical stability (BPM motion < 1  $\mu\text{m}$ )
  - TE mode suppression
  - High power (Photon absorber, RF bellows)
- Some vacuum related experiences
  - IVU problem
  - Breakdown of MCTL (Multi Chanel Transfer Line)
  - Other faults

# Location





# Pohang Accelerator Laboratory

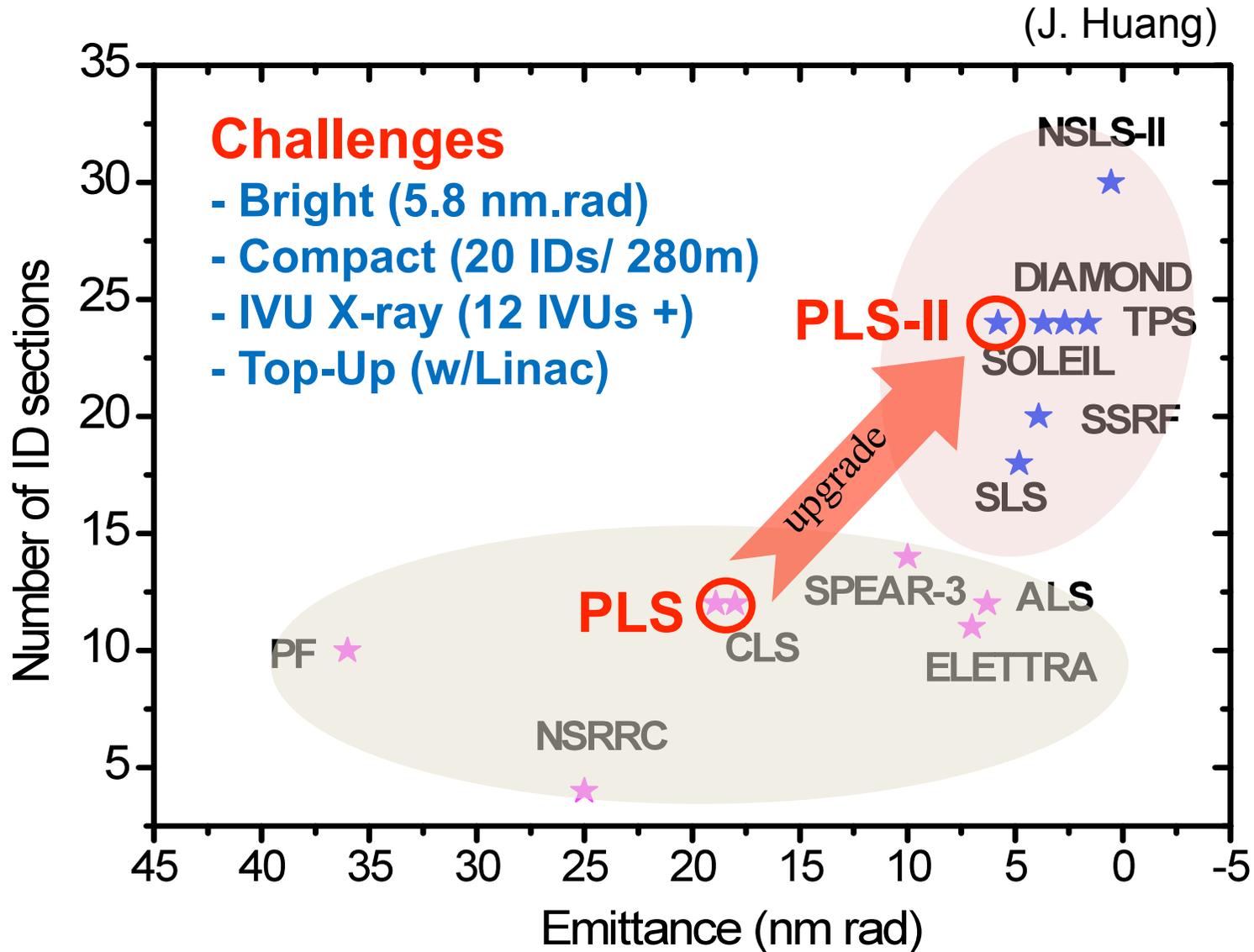




# Main parameters of PLS-II

Parameter	PLS	PLS-II	Remark
<b>Beam energy</b>	2.5	<b>3</b>	GeV
<b>Beam current</b>	190	<b>400</b>	mA
Revolution freq.	1.06855	1.06377	MHz
No of bunches	300	400	
Bunch Charge	0.59	0.94	nC (Calculated)
Bunch length	30	20	ps (Designed)
Bunch current	8.86	18.74	A (Peak value)
<b>Emittance</b>	18.9	<b>5.8</b>	nm mrad
<b>Lattice</b>	TBA	DBA	<b>20 IDs</b> (10 IDs in PLS )
Circumference	280	280	m

# Challenges of PLS-II





# Challenges of PLS-II vacuum system

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- **High heat load**
  - **417 kW**
  - **Complicated design of photon absorbers**
  
- **Tight space (Compact ring & DBA lattice)**
  - **Be built in existing building (288 m ring)**
  - **Limited space for vacuum components**
  
- **High mechanical stability**
  - **< 1  $\mu\text{m}$  (rms)**
  - **Ground motion**
  - **Thermo mechanical effect**

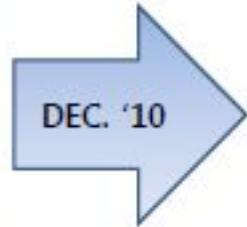


# Re-installation of PLS-II storage ring

PLS



Dismantling



Re-  
installation



Jun. '11



# PLS-II timeline

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## ○ 2011

- 25 January, PLS-II installation begins
- 23 May, Linac commissioning begins
- 13 June, 3 GeV beam
- 25 June, SR installation finished
- 1 July, First turn
- 5 July, Kicker PS accident
- 5 August, First accumulation
- 7 October, 100 mA stored
- 24 October, First photons to beamline

## ○ 2012

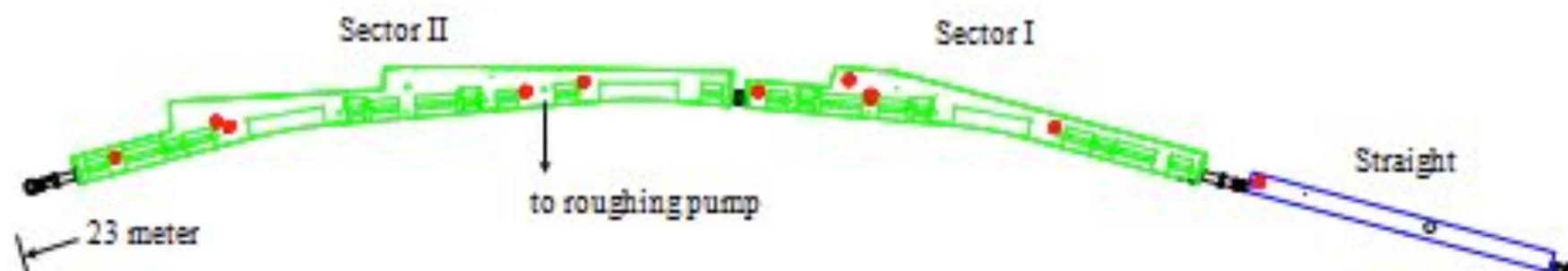
- 14 February, Commissioning with users
- 21 March, Start of operations

## ○ 2013

- 18, Jun, 200 mA top-up operation

## ○ 2014

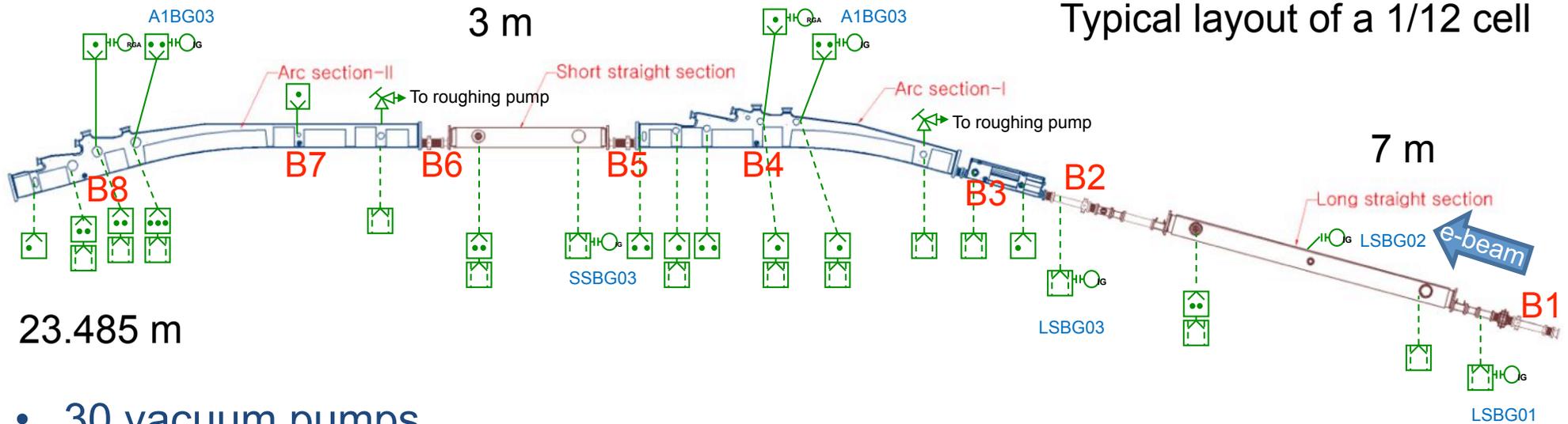
- January, MCTL break down (2 months for repair)
- October, IVU foil bump (3 IVUs)
- December, 400 mA top-up operation



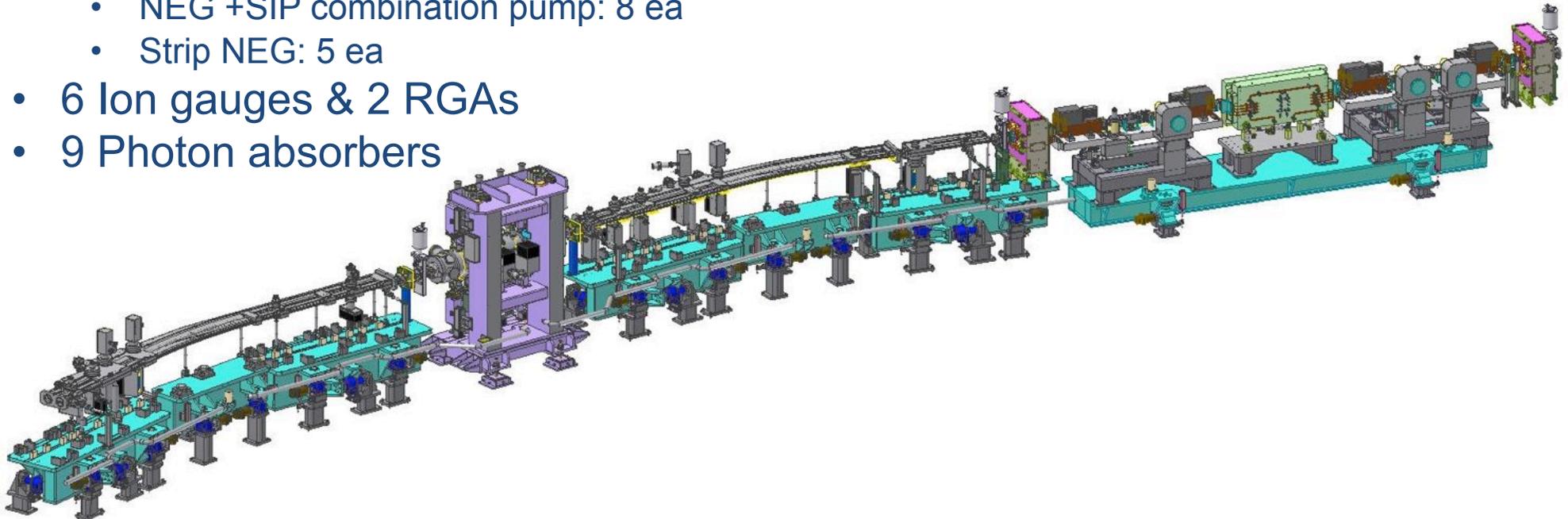
- ◆ Chamber material
  - *A5083-H321 (Machined)*
  - *A6063-T5 (Extruded)*
  - *Stainless Steel 304L/316*
- ◆ Photon absorber; *OFHC Cu*
- ◆ Roughing pump
  - *Magnetic turbo + dry pump*
- ◆ Main vacuum pump
  - *SIP; 10 \* 60 l/s*
  - *NEG(ST707); 19 \* WP950*



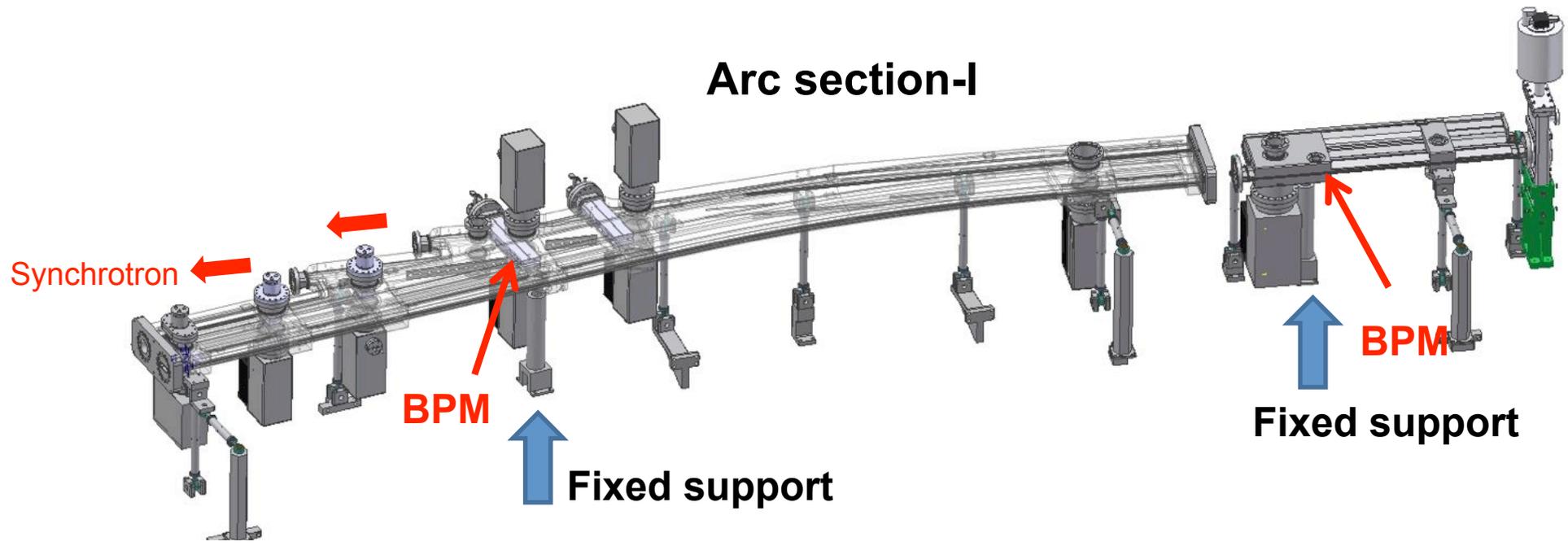
# Layout of PLS-II storage ring vacuum system



- 30 vacuum pumps
  - Sputter ion pumps (30 l/s + 60 l/s): 7 ea
  - Lumped NEG (WP950 + D-400-2): 9 ea
  - NEG +SIP combination pump: 8 ea
  - Strip NEG: 5 ea
- 6 Ion gauges & 2 RGAs
- 9 Photon absorbers

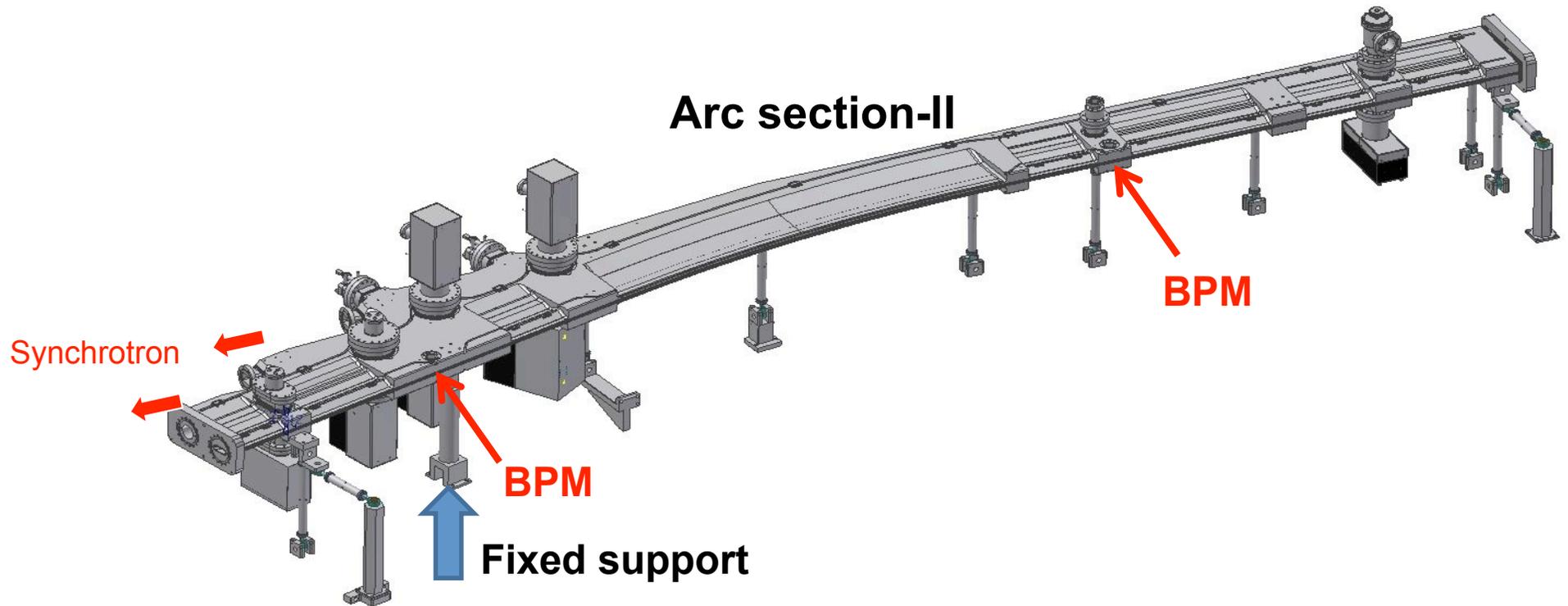


### Arc section-I



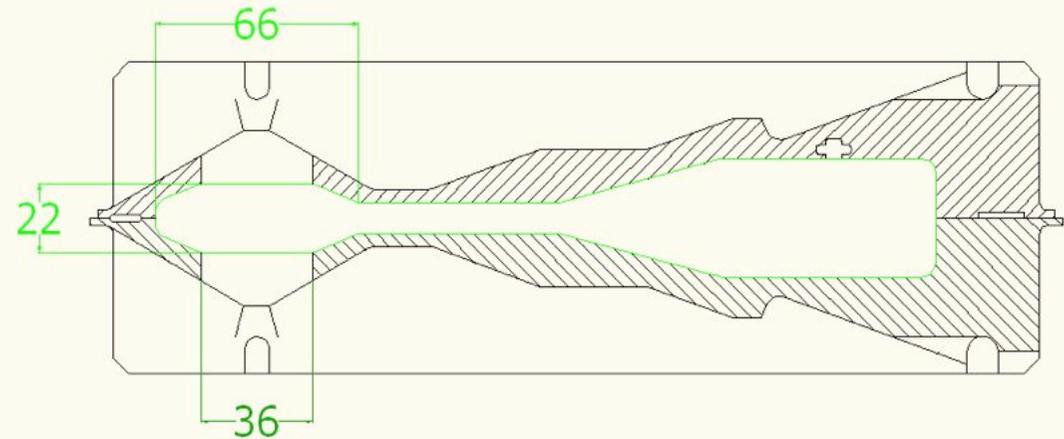
## Chamber & supports (Arc section)

### Arc section-II



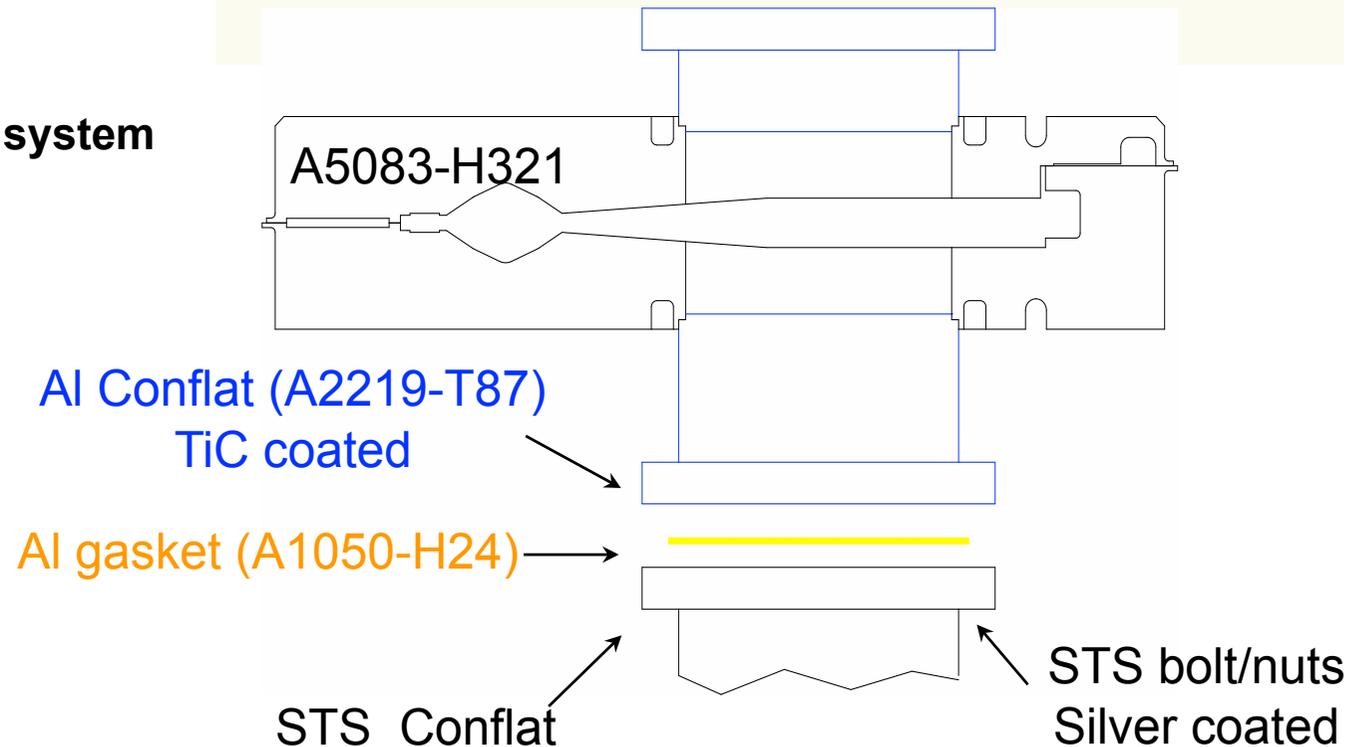
# Arc-section vacuum chamber

- **Cross section**



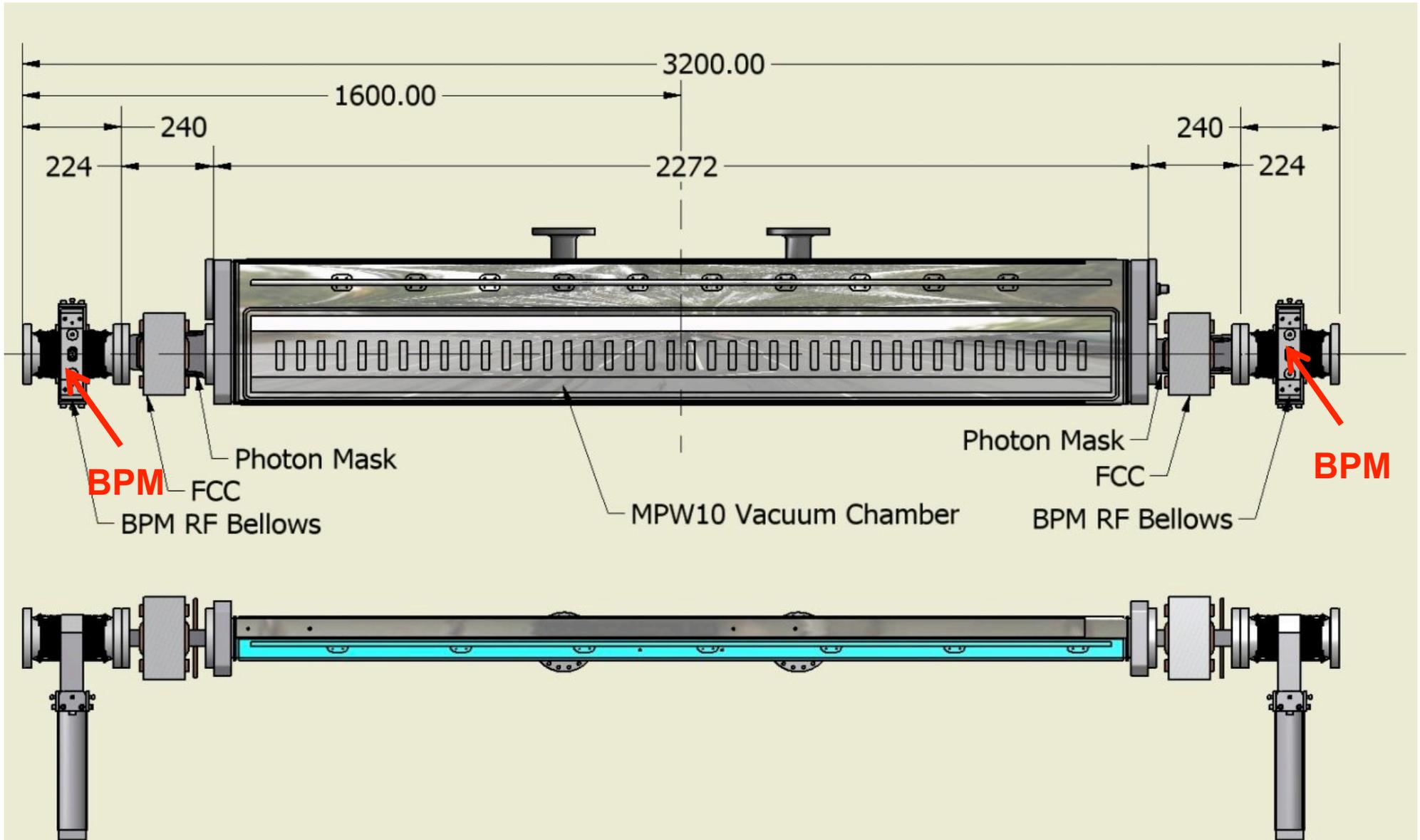
- **Vacuum seals**

- Al/SUS hybrid Conflat system

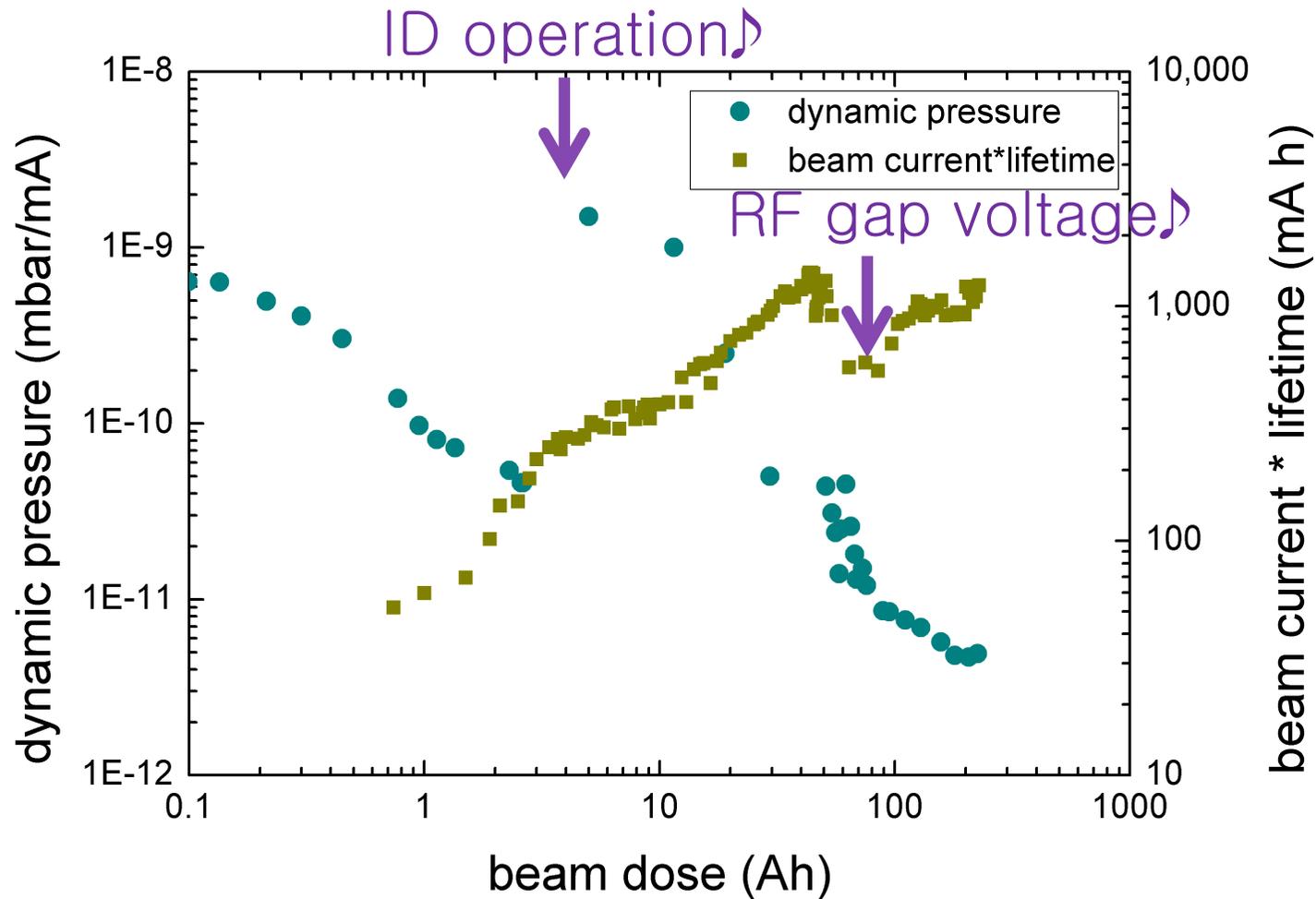




# Chamber supports (Short straight section)



# Pressure and lifetime in the early stage



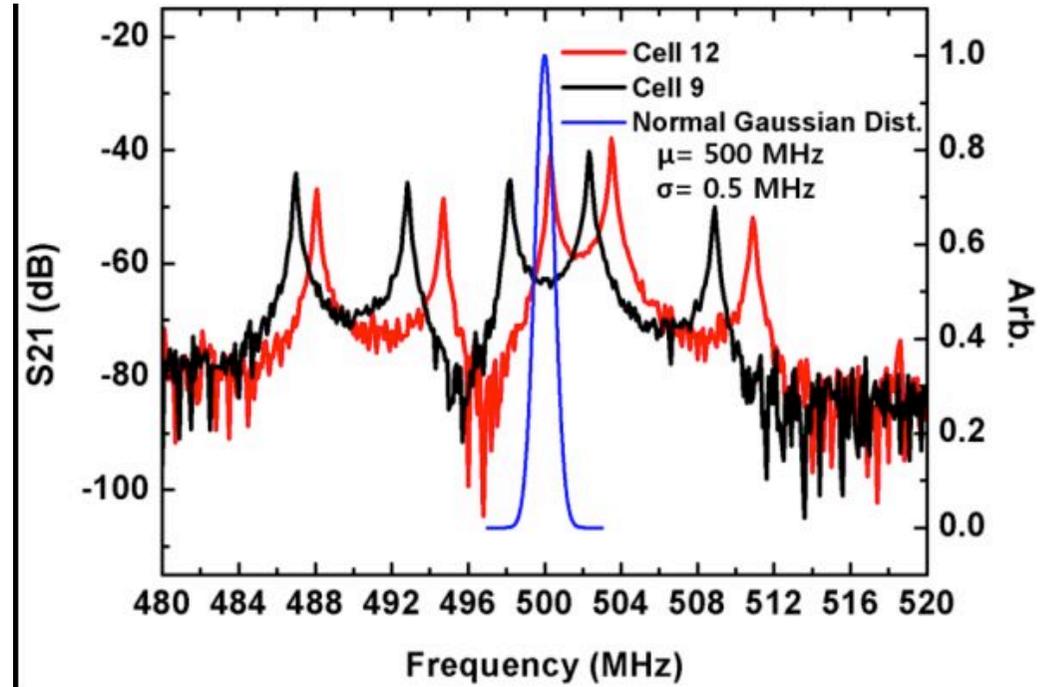
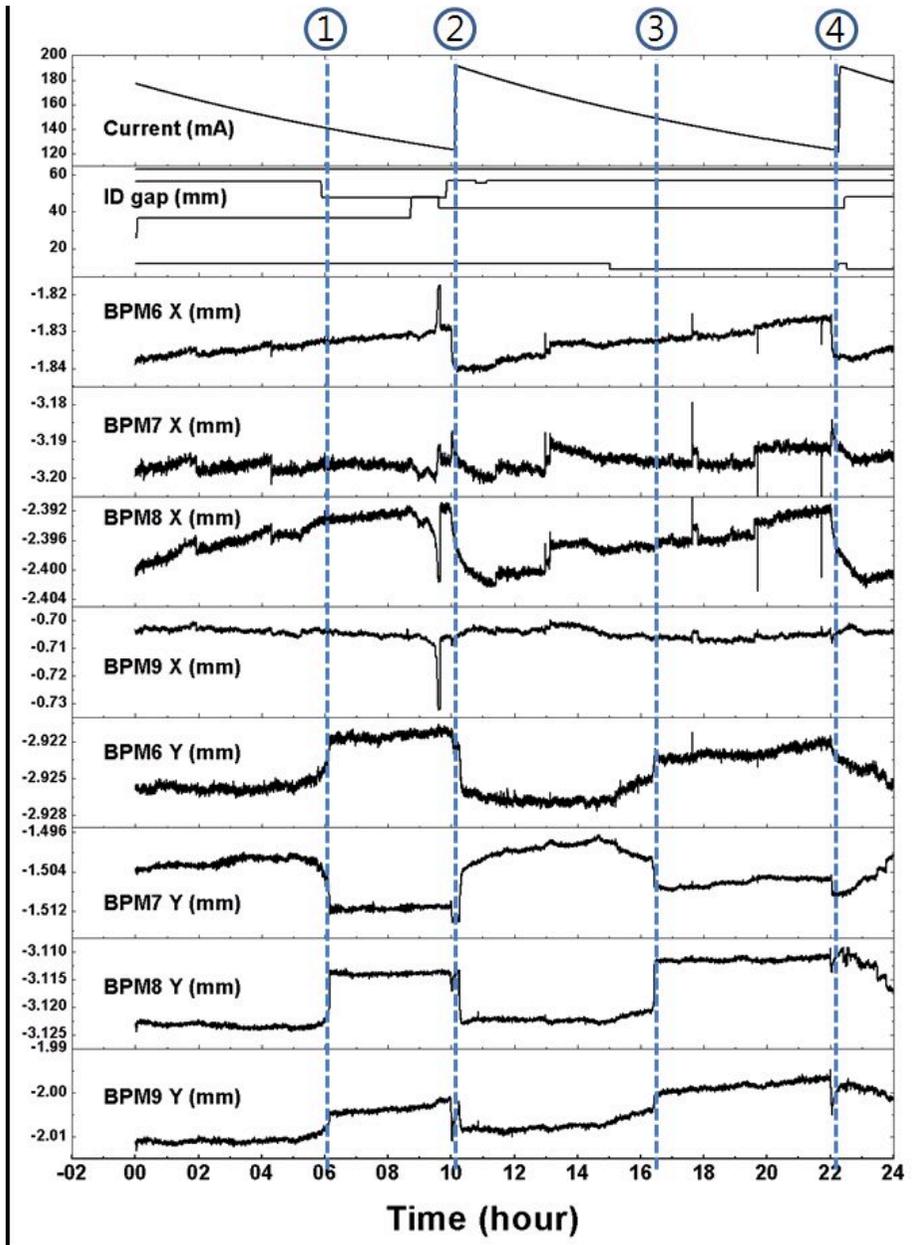
- Dynamic pressure reached to  $<10^{-11}$  mbar/mA after integrated beam current of 50 Ah which is our target value.
- Beam-gas scattering lifetime dominates at the early stage of commissioning. After ~50 Ah, Touscheck effect mainly limits beam lifetime.

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# TE mode suppression



# TE mode excited in PLS SR chamber



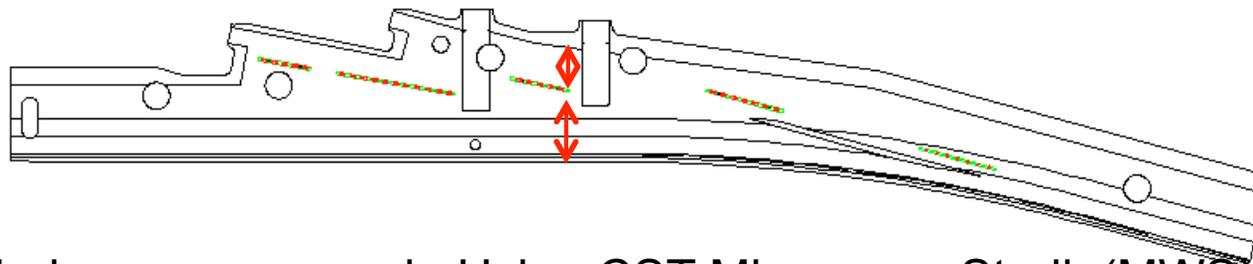


# Shunt structure to avoid TE mode in PLS-II Vacuum chamber

## Design Goal

→ No resonance mode in the frequency band of  $500 \pm 5$  MHz

## How to ?



Find resonance mode Using CST Microwave Studio(MWS)  
Shunt structure (stiffener)  
→ Reduce effective width  
→ Control of frequency of TE modes

Val seal for RF contact

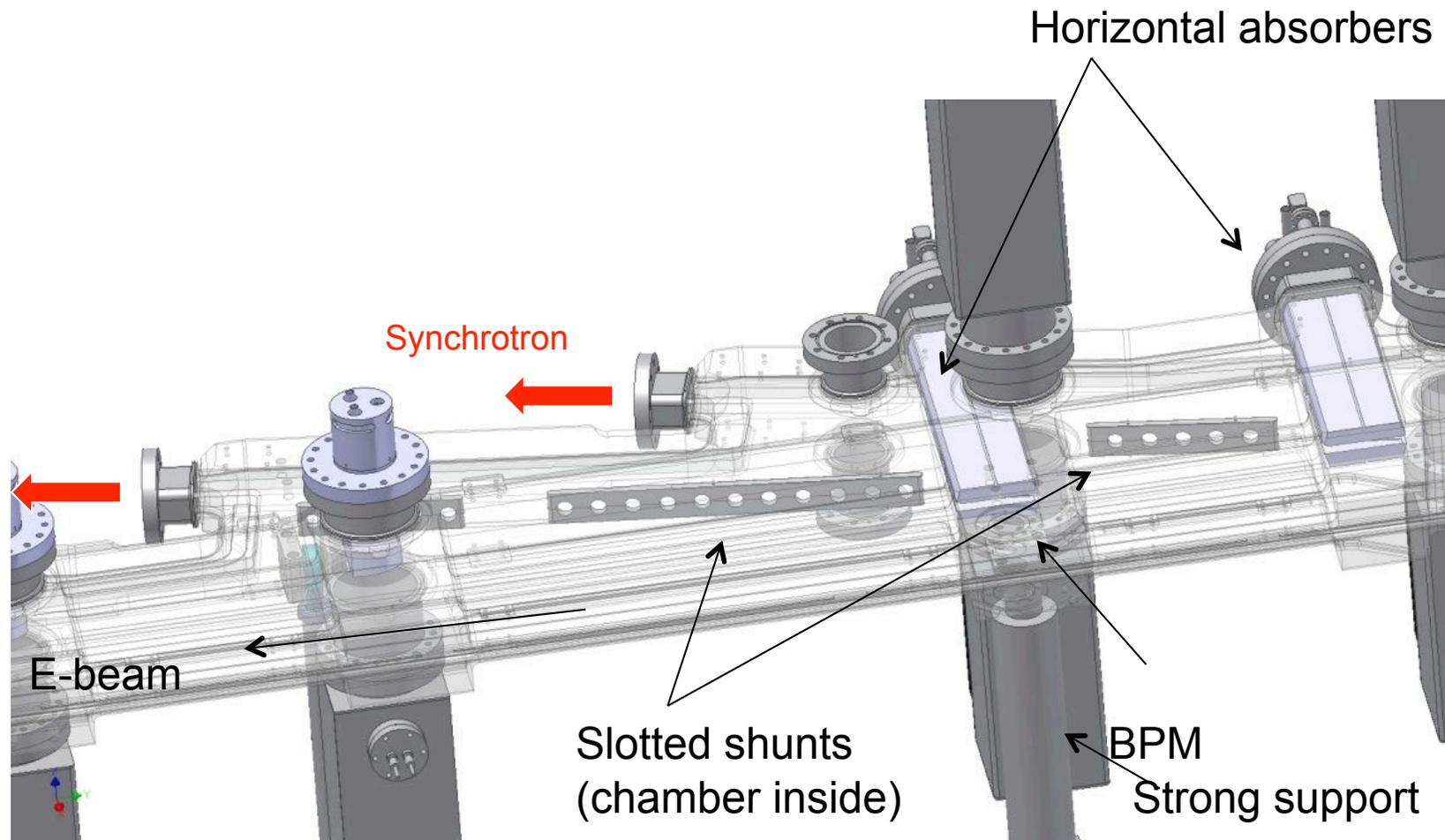
Holes for vacuum pumping



Bolt connection to plate

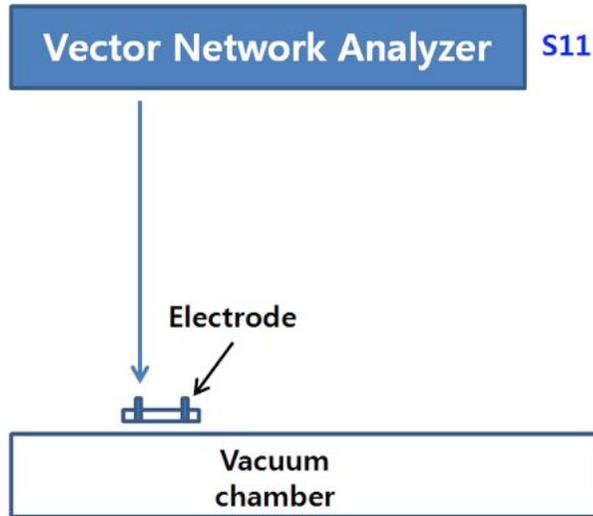
# SR vacuum chamber assembled

- To control the resonance mode frequency
  - Slotted stiffeners are installed to minimize conductance reduction

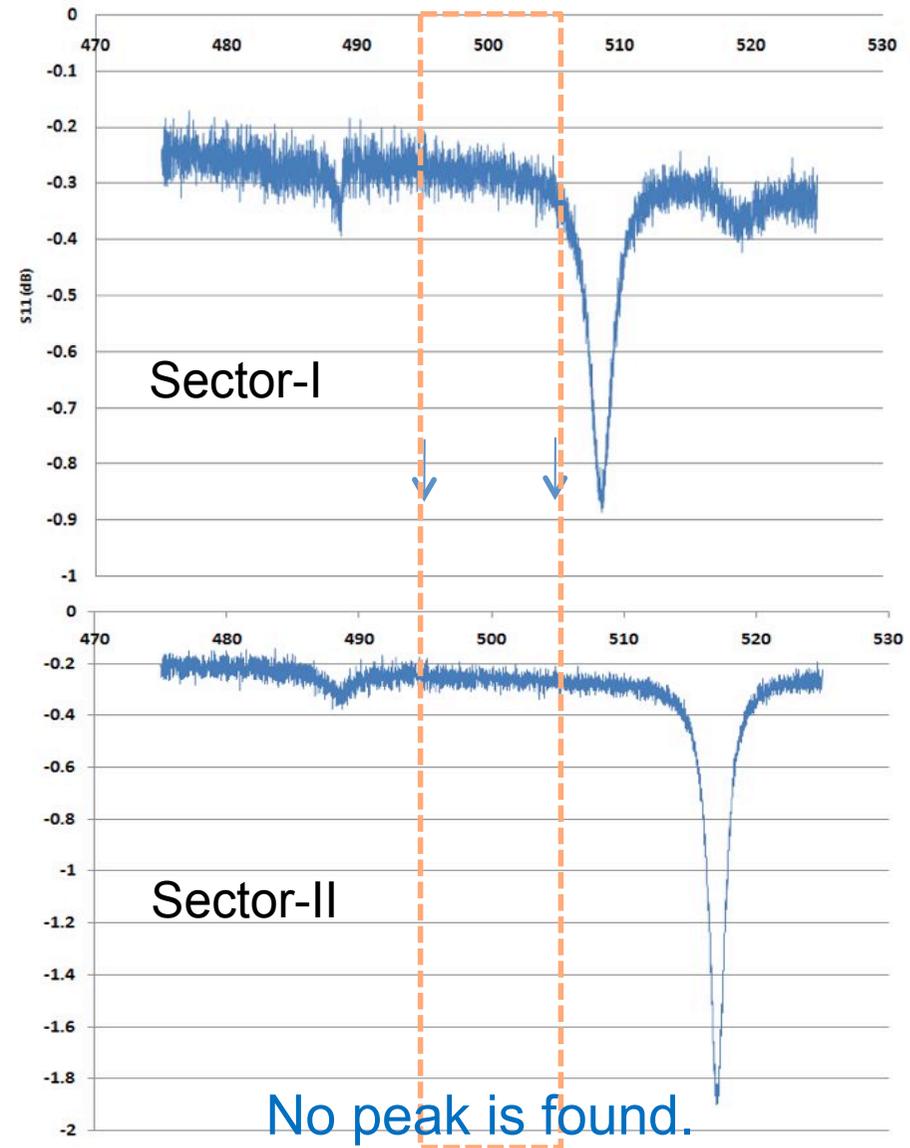


# TE mode measurement results

- Setup and Results



Pickup antenna on BPM electrode



**No TE mode found in PLS-II operation mode until now!**

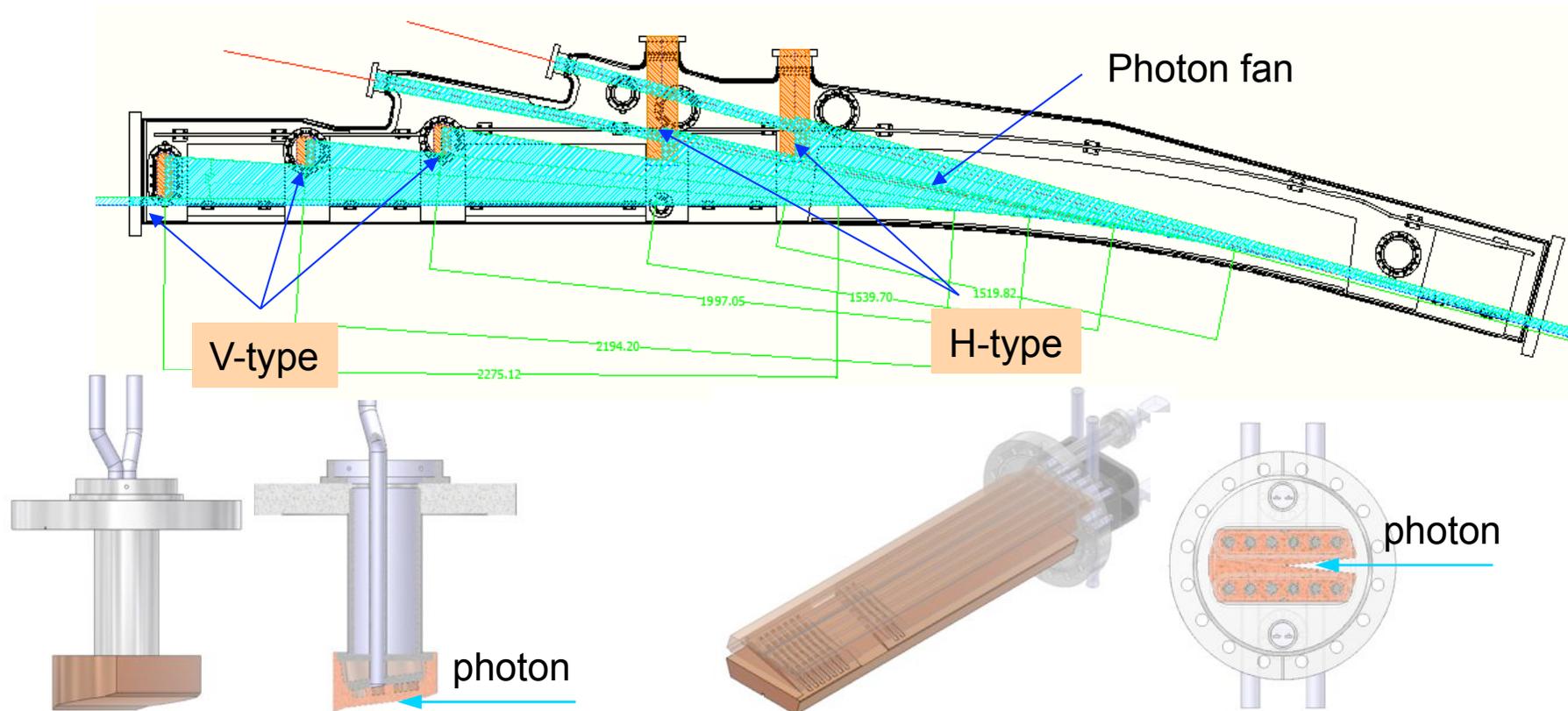
# **Photon absorber & RF bellows**

# Photon absorbers in PLS-II

- Total synchrotron radiation power is increased from 110 kW to 417 kW.

$$P[kW] = 88.463 \cdot \frac{E[GeV]^4}{\rho[m]} \cdot I[A] \quad (17 \text{ kW per bending magnet})$$

- ✓  $E=2.5 \text{ GeV}$ ,  $I=200 \text{ mA}$ ,  $\rho=6.306 \text{ m}$  (PLS)
- ✓  $E=3.0 \text{ GeV}$ ,  $I=400 \text{ mA}$ ,  $\rho=6.875 \text{ m}$  (PLS-II)





# Parameters for PA design

Item	Magnitude	Unit
Beam energy ( $E$ )	3	GeV
Beam current ( $I$ )	400	mA
Bending radius( $\rho$ )	6.8775	m
Bending magnet field ( $B$ )	1.4557	T
Total power	417	kW
Beam divergence (1/gamma)	0.17	mrاد

Input Parameters	Magnitude	Unit
Source distance	1520	mm
Incident peak power density	12.23	W/mm <sup>2</sup>
Rectangular approximation width	0.405	mm
Convection film coefficient	1	W/cm <sup>2</sup> K
Vertical miss-steering	±1.5 mm offset	



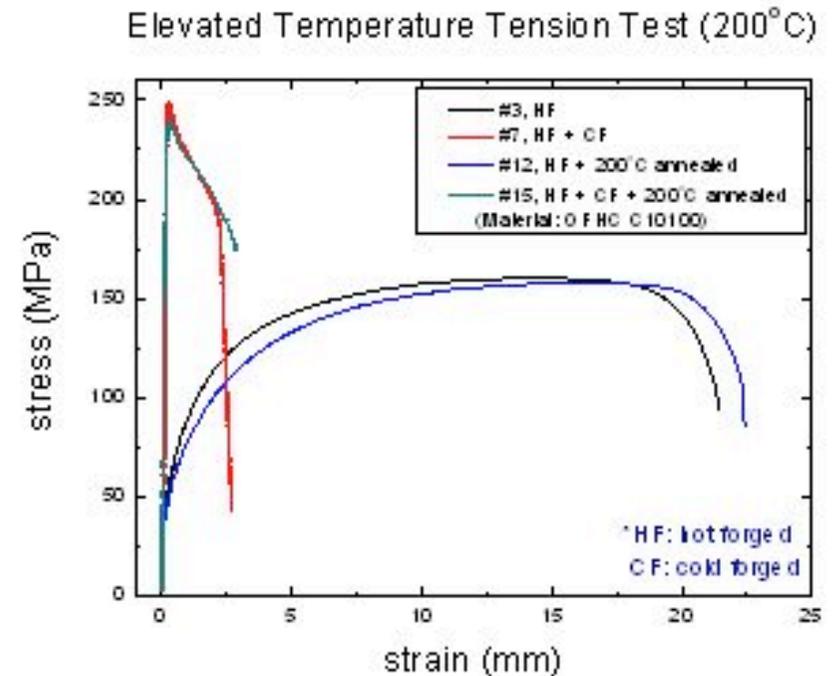
# Materials for PA (cold forged OFHC)

## Material

- OFHC
  - ✓ High thermal conductivity
  - ✓ E-beam welding
  - ✓ Easily available than Glidcop

- Elevated temperature (200°C) tension test

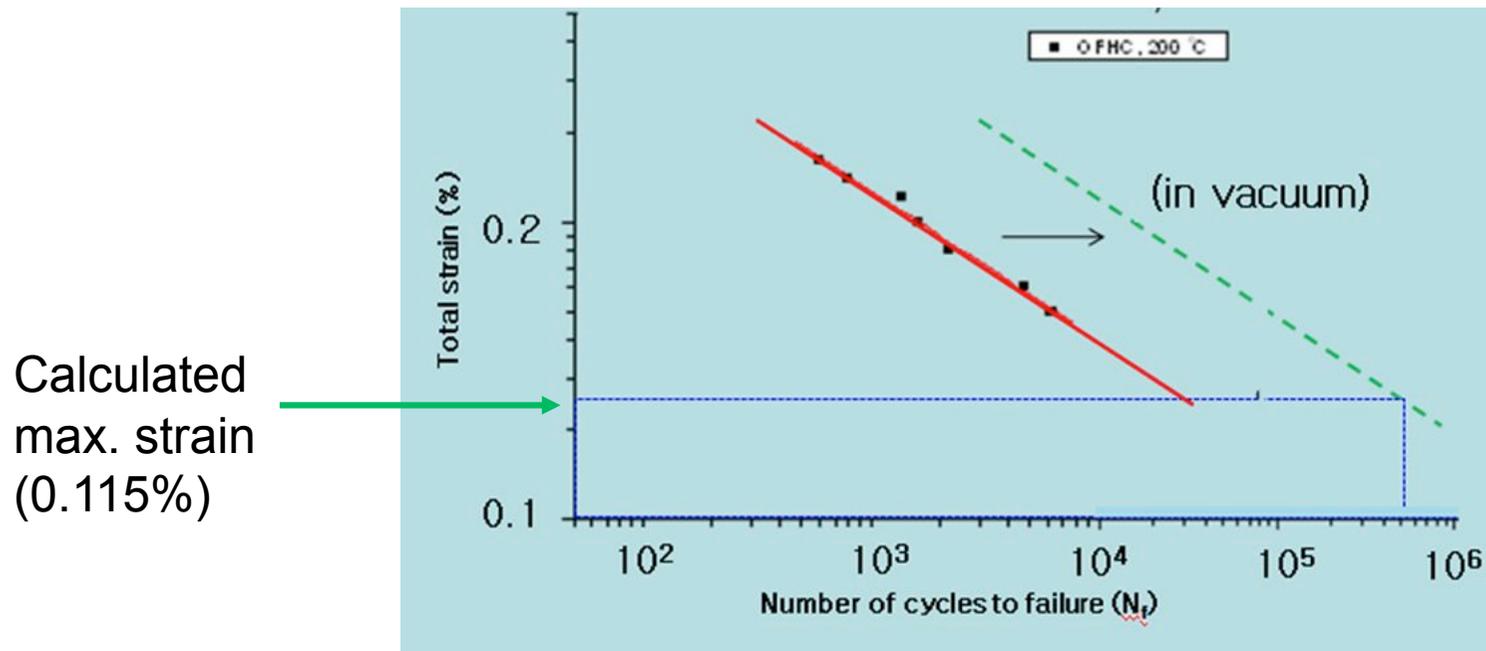
Material process	YS(0.2%) / MPa	TS / MPa	EL / %
Hot forged (OFHC)	48.3	160.3	42.4
Hot + Cold forged	244.4	249.1	5.2
HF + 200°C Annealed	48.9	157.7	43.9
<b>HF + CF + 200°C Annealed</b>	<b>240.0</b>	<b>240.3</b>	<b>5.8</b>



- The yield strength of the cold forged OFHC is enhanced up to 240 MPa.

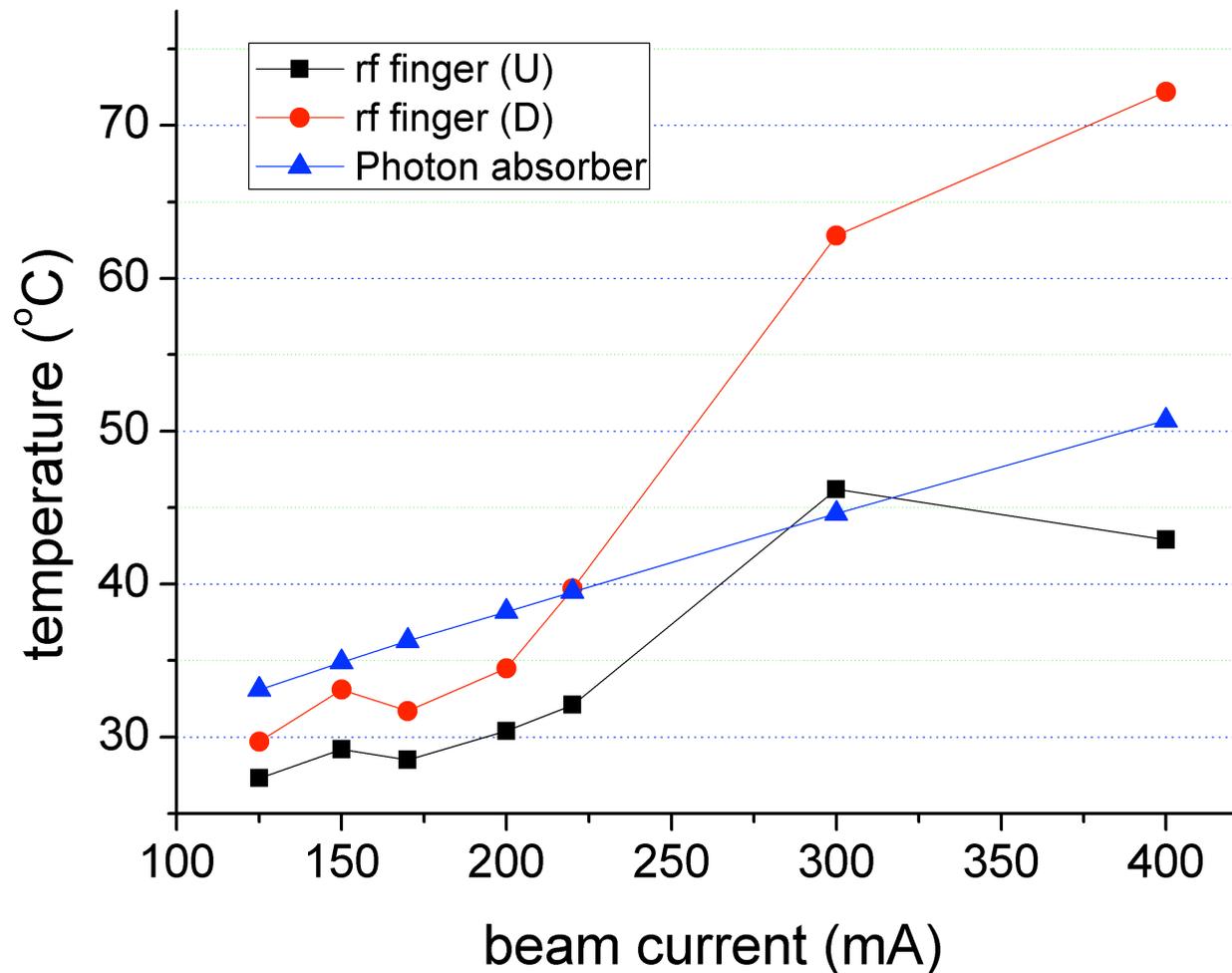
# Materials for PA (cold forged OFHC)

## Lifetime measurement



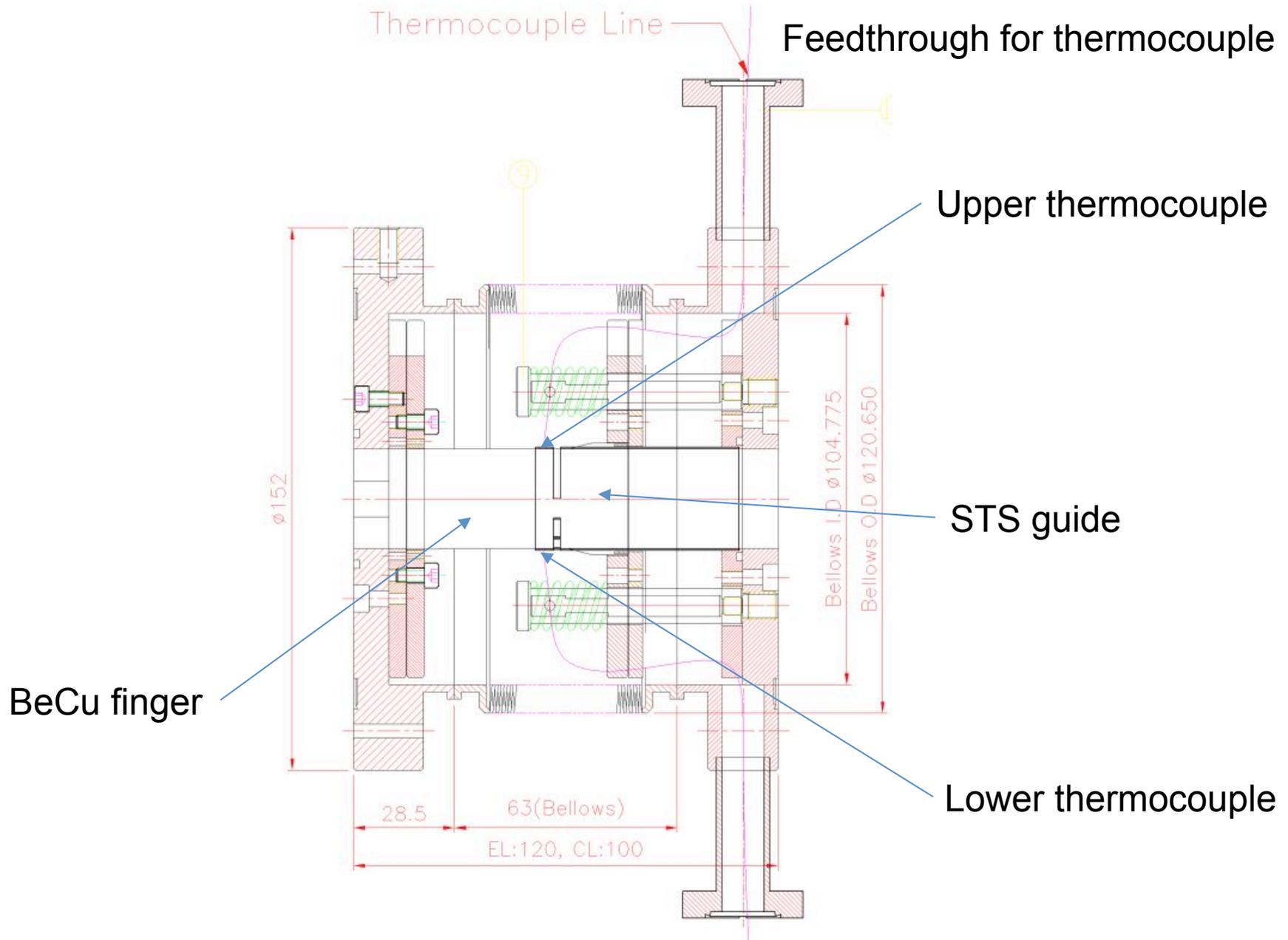
- Number of cycles to failure for total strain of 0.115 % (most severe point) in air is measured to be larger than 10,000 cycles
- Fatigue lifetime in vacuum is 10 times longer than that in air, typically.
- The lifetime of the PLS-II photon absorber is expected to be longer than 100,000 cycles

# Photon absorber in operation



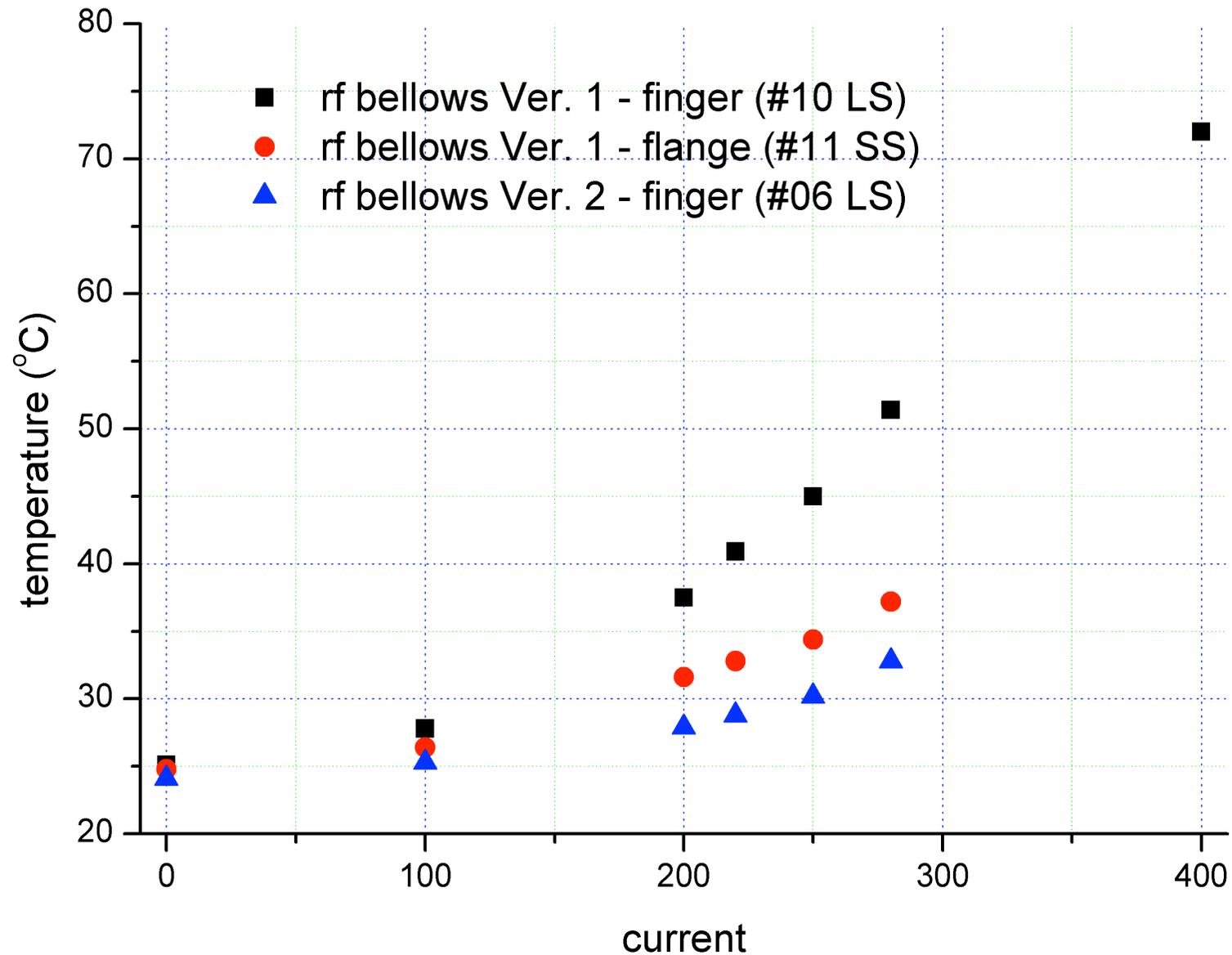
- Operating temperature of the most severe photon absorber at the sensor position is measured to be 50°C at 400 mA.
- Most severe point ~ 150°C at 400 mA (much lower than the thermal analysis result)

# RF shielded bellows





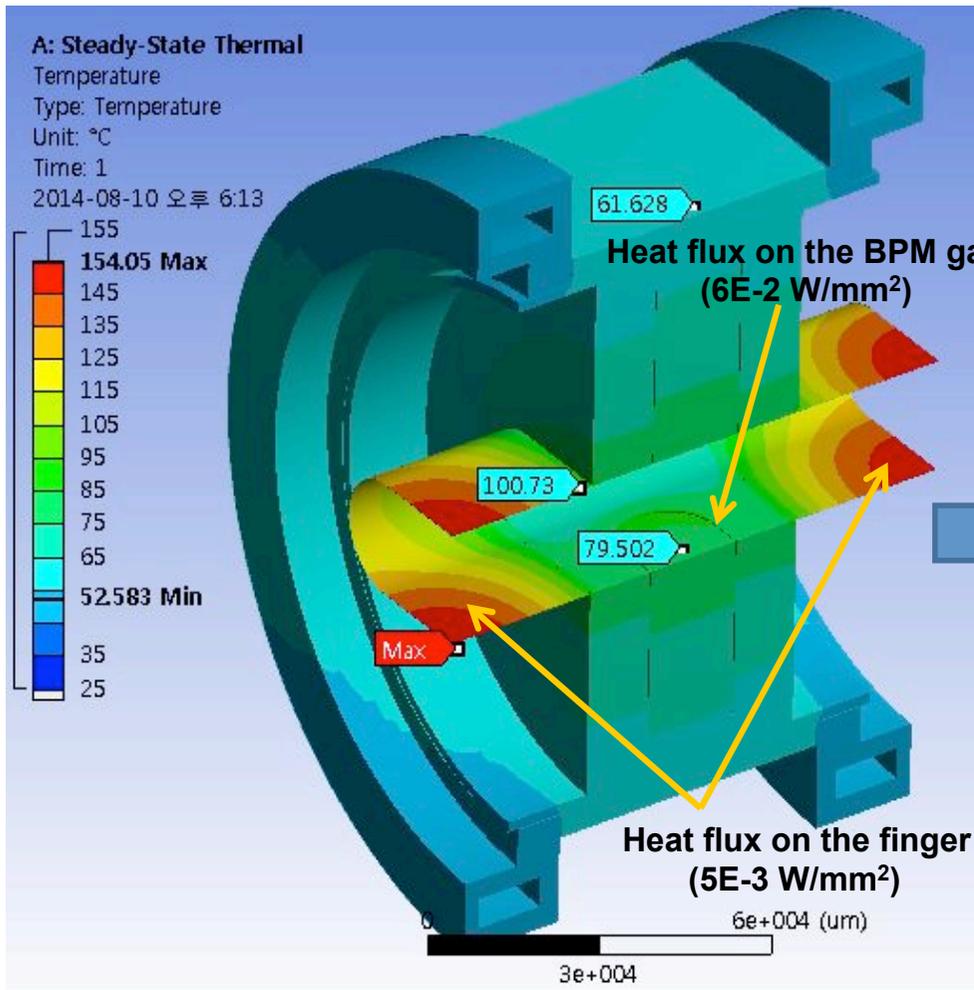
# RF shielded bellows in operation



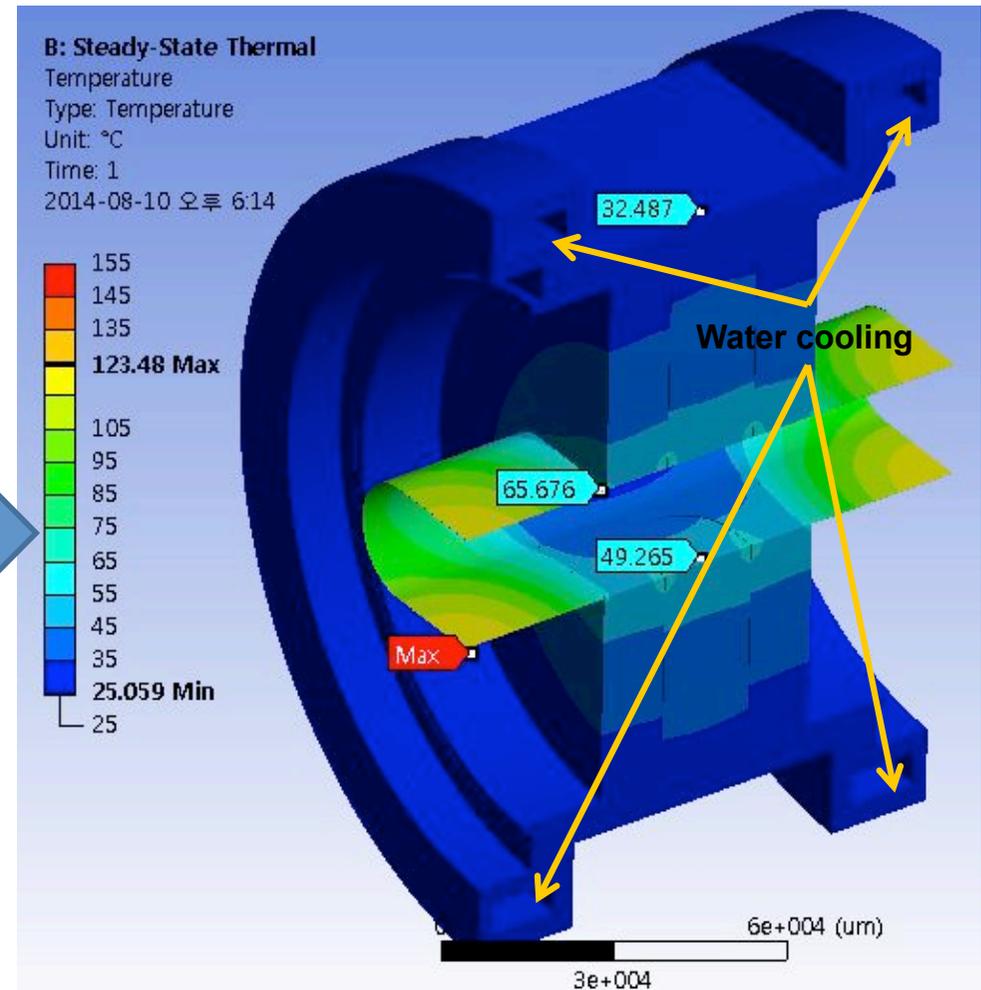


# Thermal analysis of BPM-bellows module

- Temperature @ 400 mA (appropriate heat flux was assumed)
  - Water cooling reduces the temperature by  $\sim 30^{\circ}\text{C}$



Natural air convection ( $2.2\text{E}-5 \text{ W/mm}^2\text{K}$ )

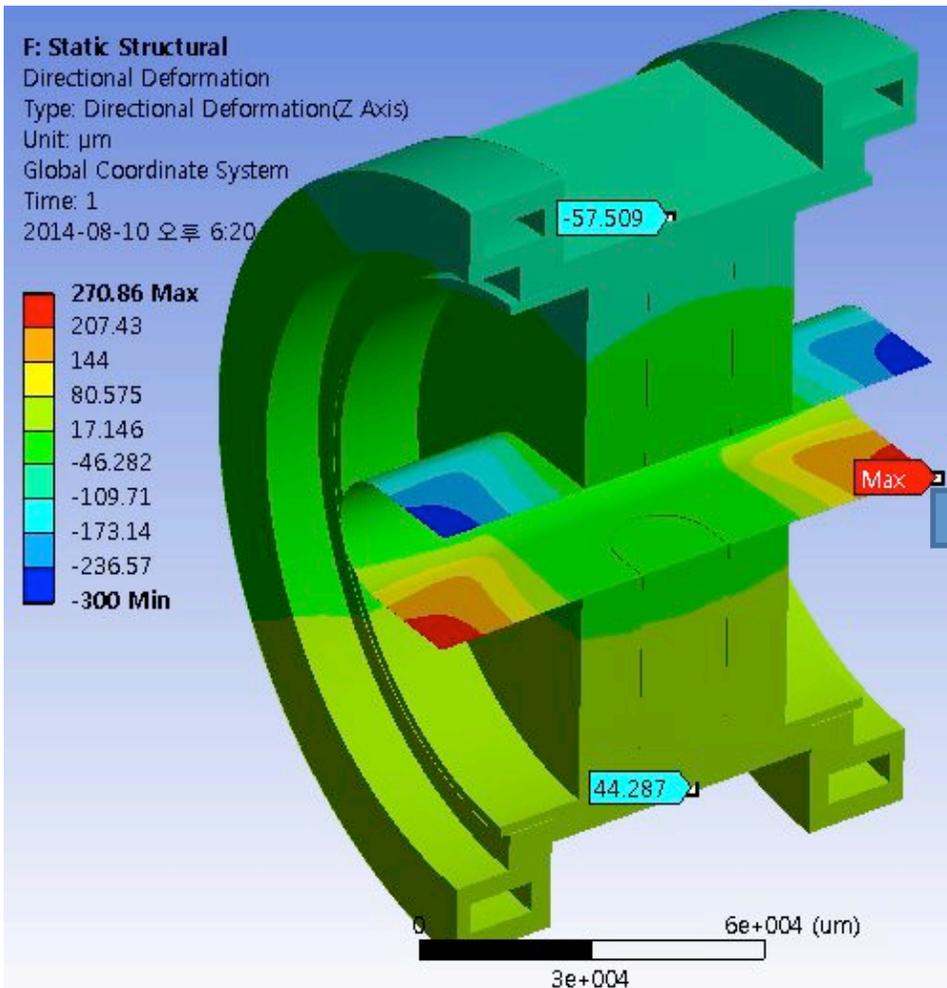


Natural air convection ( $2.2\text{E}-5 \text{ W/mm}^2\text{K}$ )  
+ Water cooling ( $1\text{E}-2 \text{ W/mm}^2\text{K}$ )

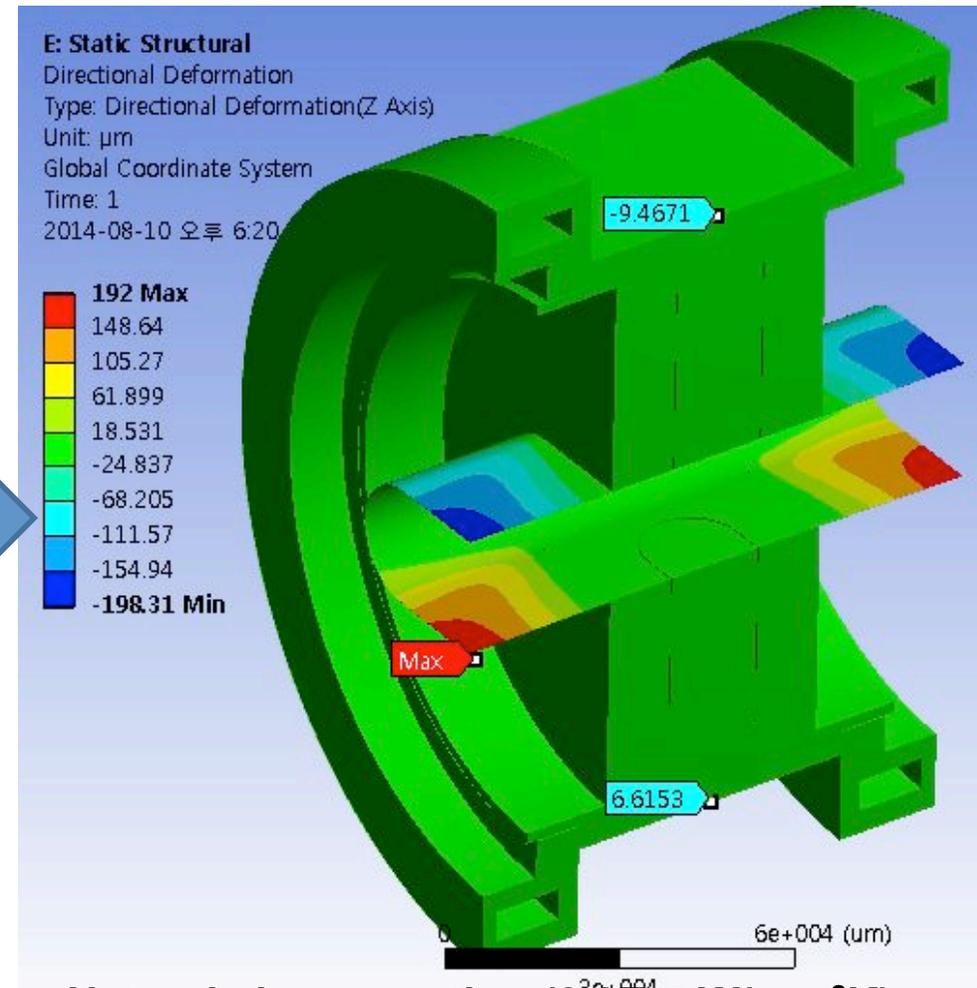


# Thermal analysis of BPM-bellows module

- Deformation @ 400 mA
  - Vertical displacement of the BPM center w/o water cooling is  $\sim 6.6 \mu\text{m}$
  - Vertical displacement of the BPM center with water cooling is  $\sim 1.4 \mu\text{m}$



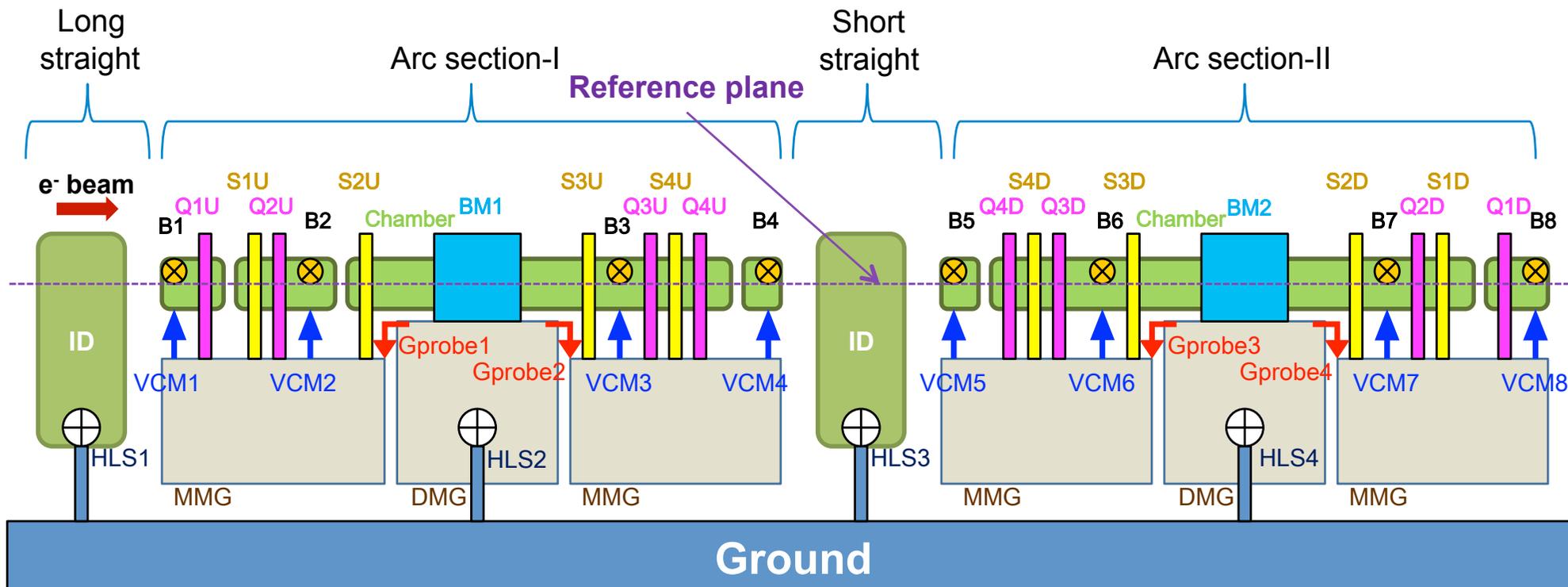
Natural air convection ( $2.2\text{E-}5 \text{ W/mm}^2\text{K}$ )



Natural air convection ( $2.2\text{E-}5 \text{ W/mm}^2\text{K}$ )  
+ Water cooling ( $1\text{E-}2 \text{ W/mm}^2\text{K}$ )

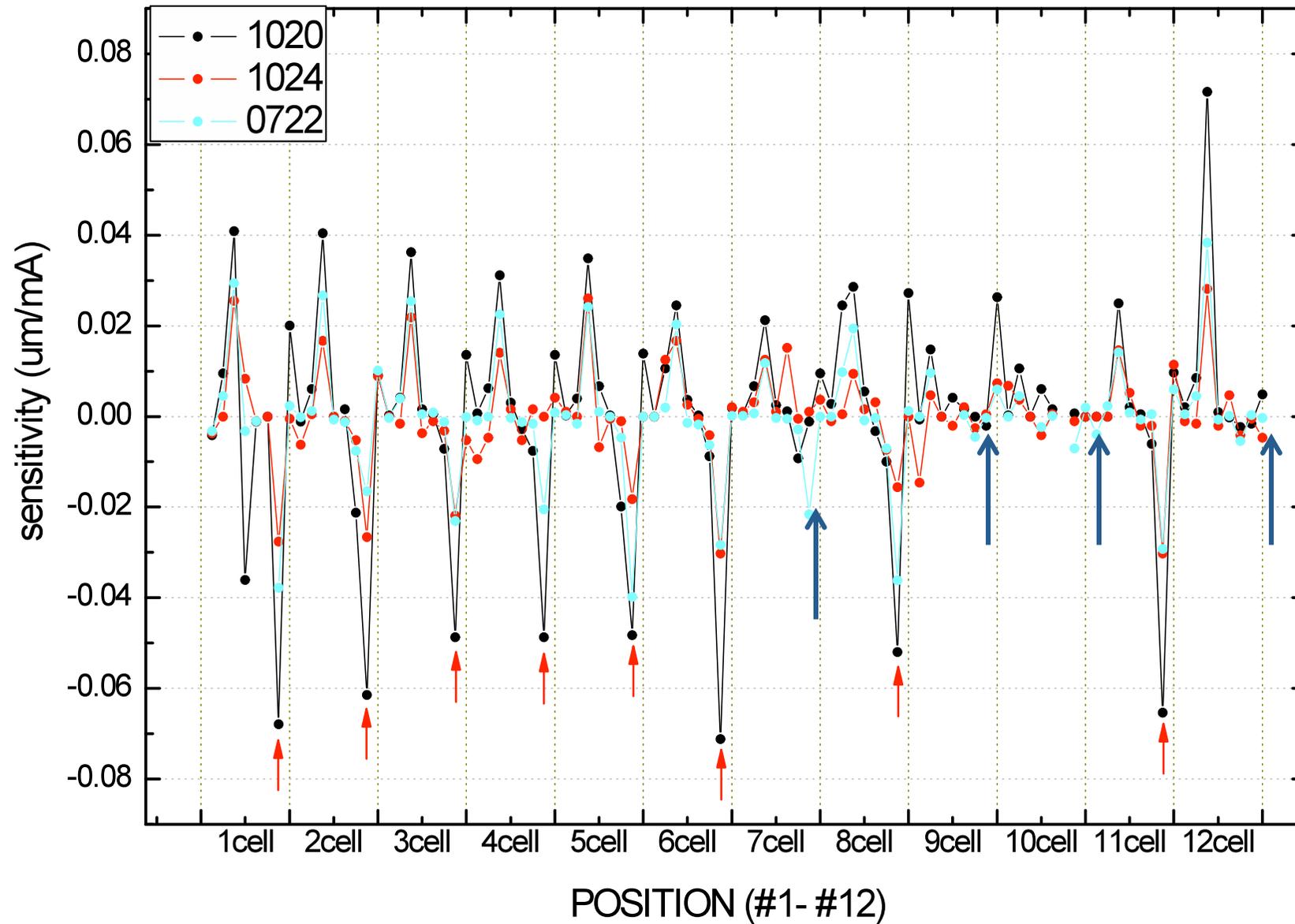
# **BPM position monitoring**

# Monitoring of BPM position

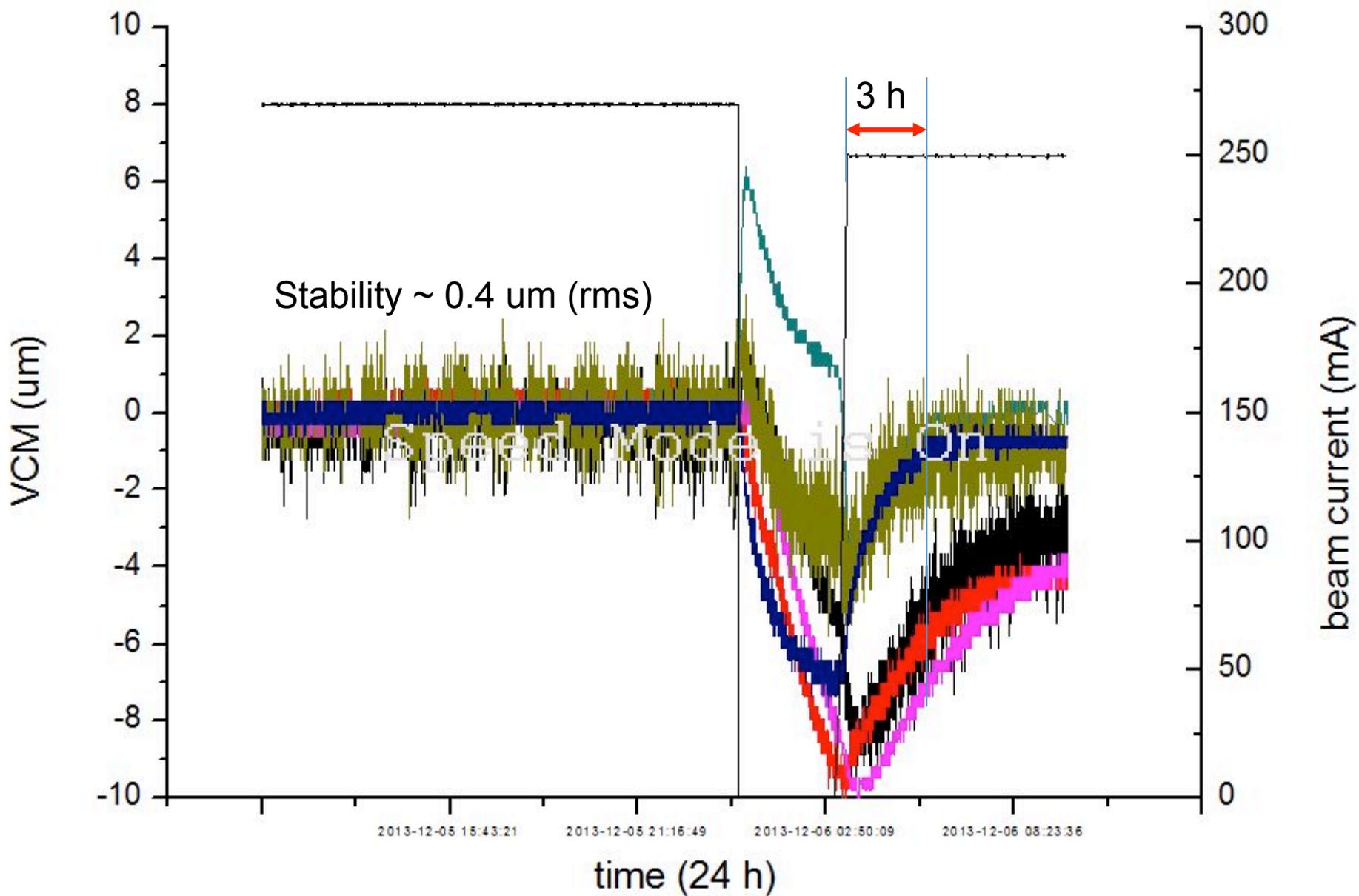


# Thermo-mechanical effect

## VCM - Beam current dependency

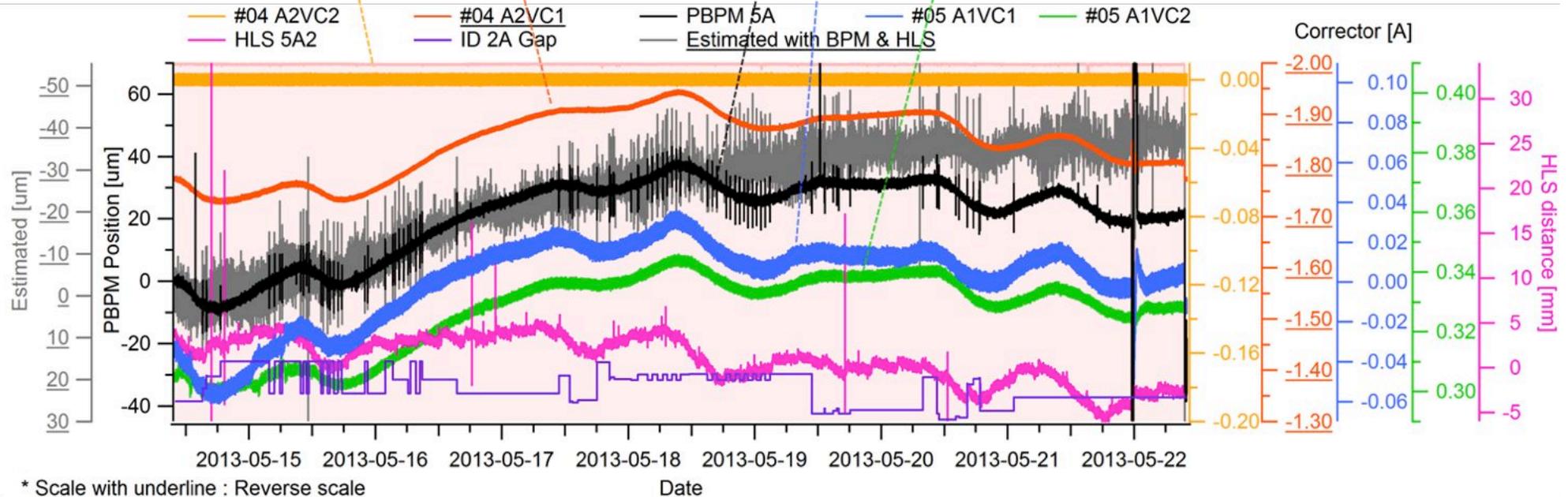
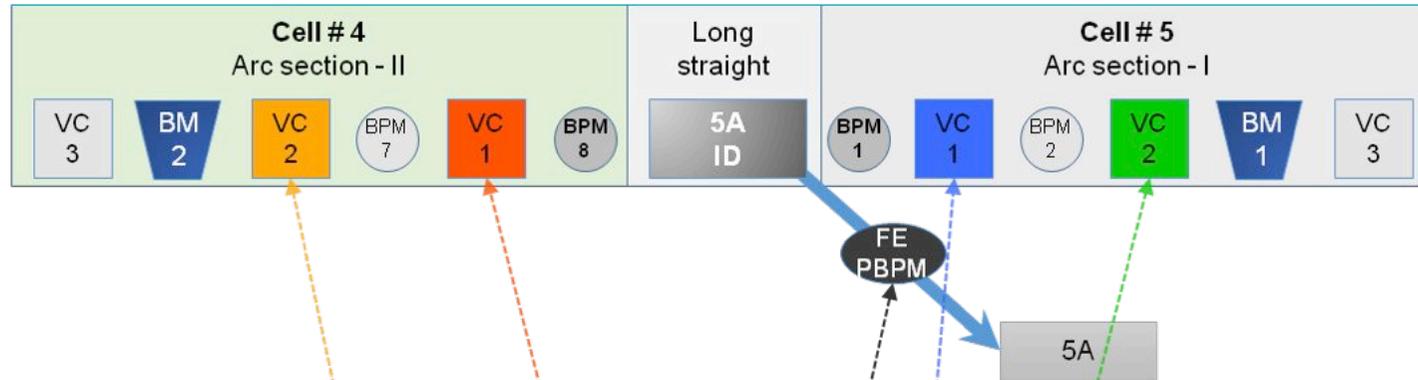


# Thermo-mechanical effect



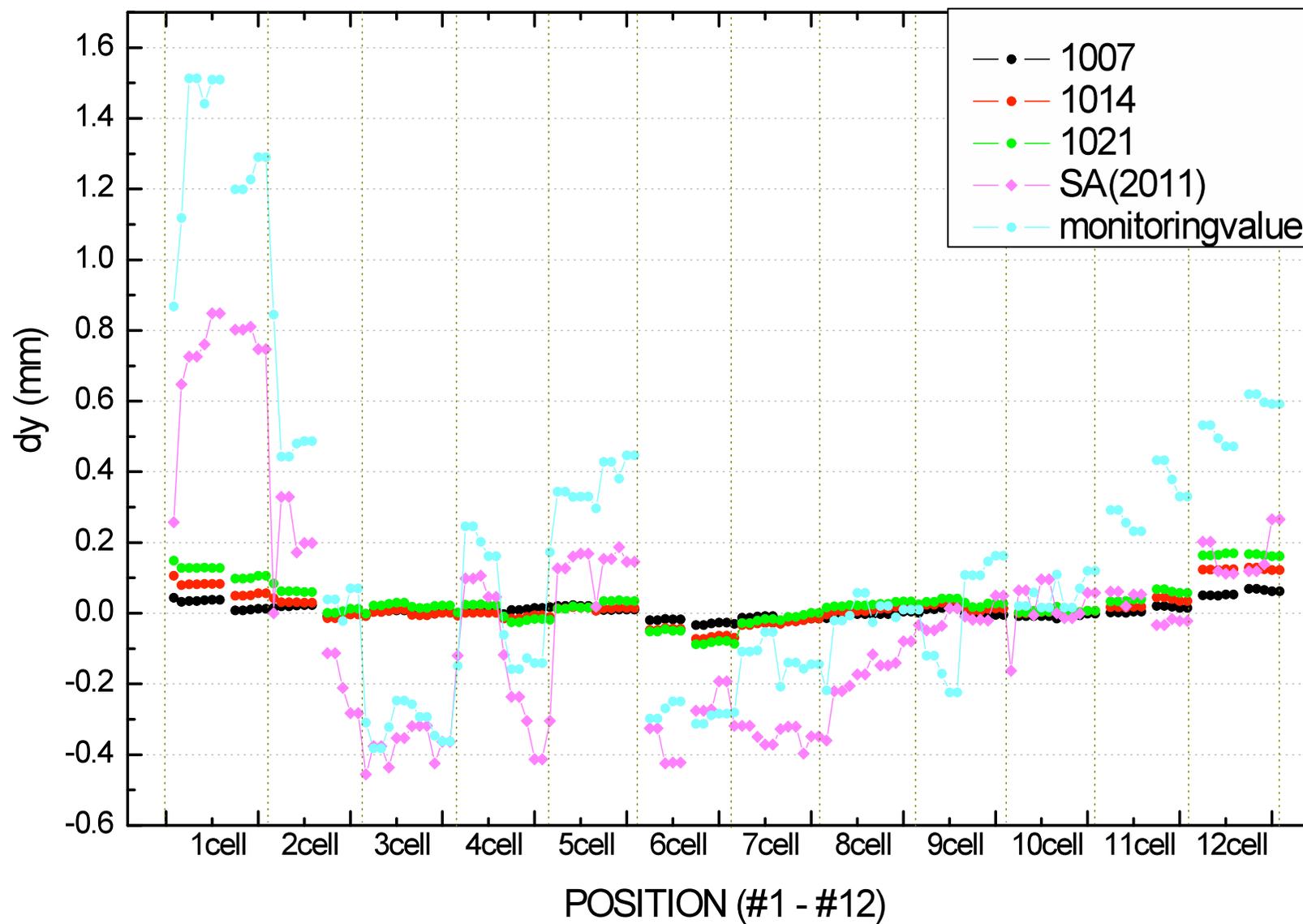


# Long term variation of photon beam

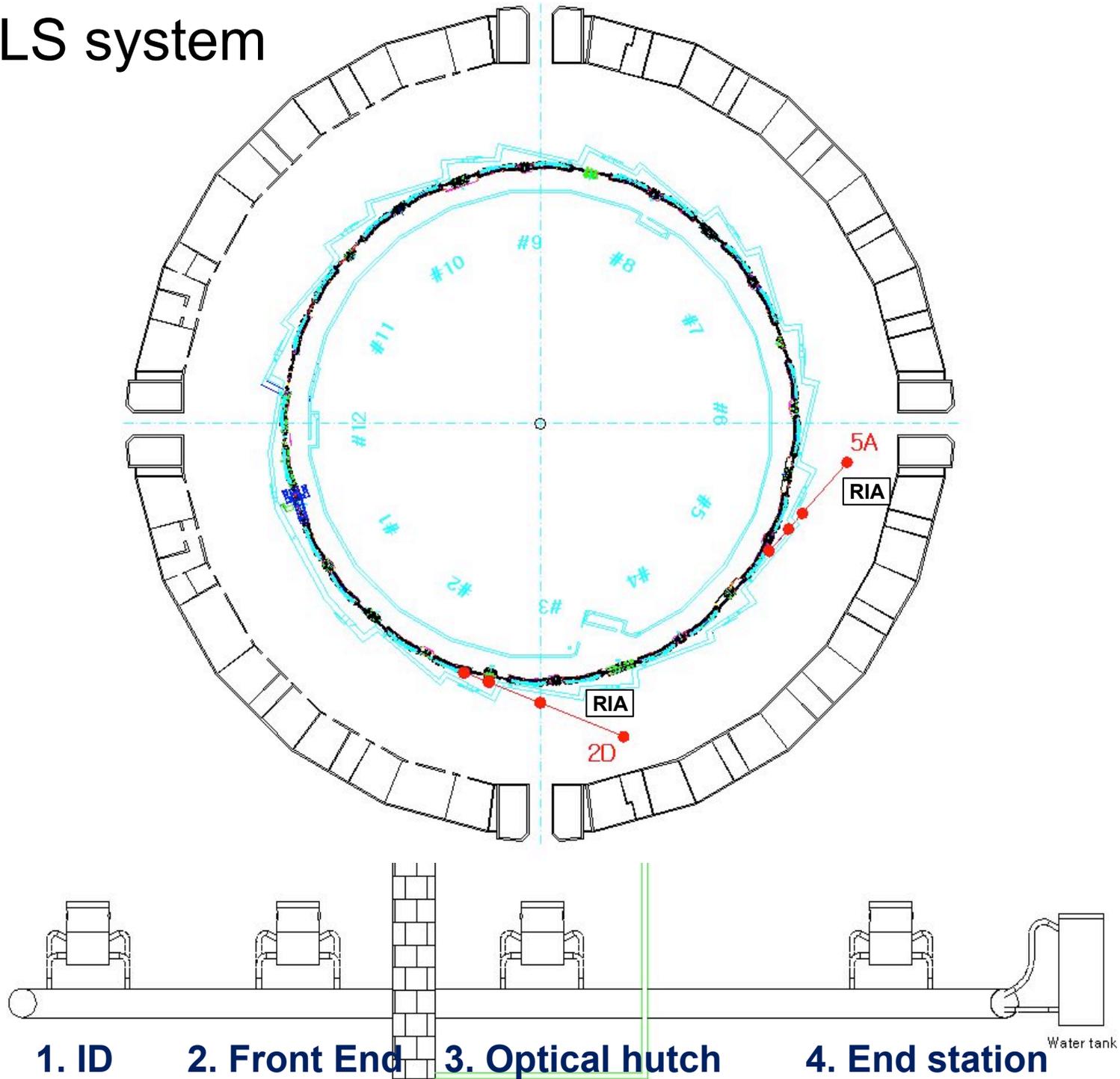


# Ground motion

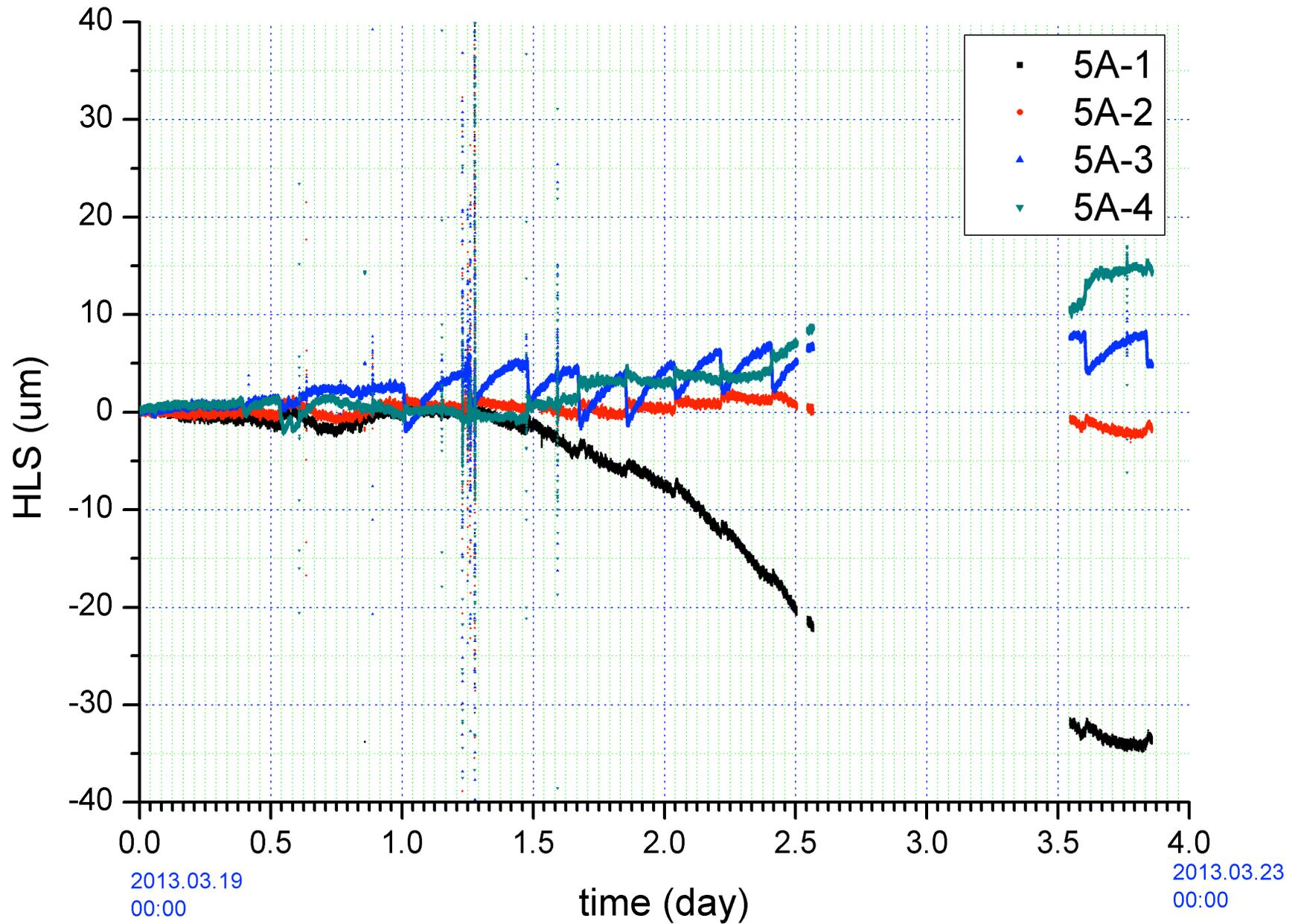
Measured by HLS



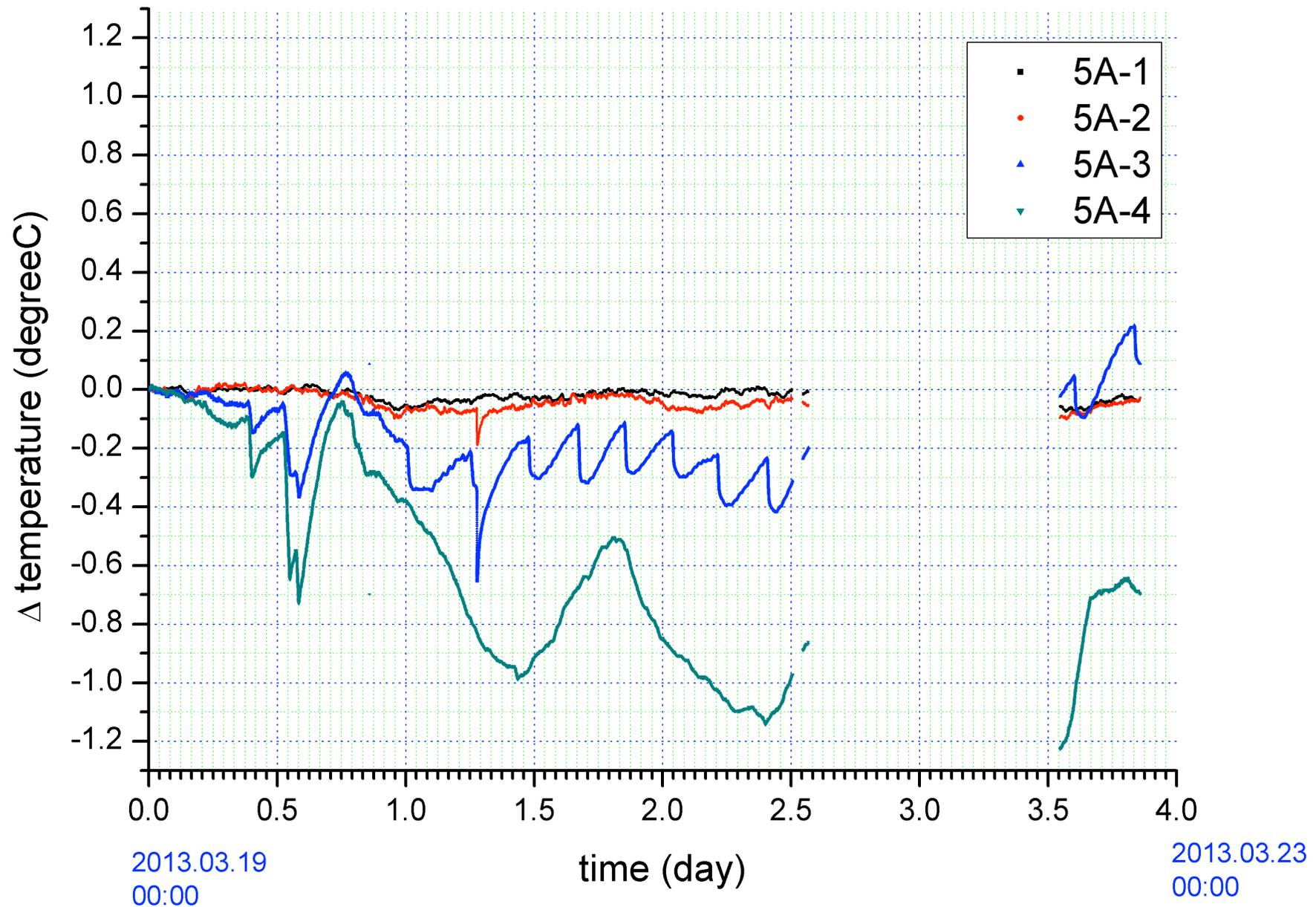
# HLS system



# 5A beam line HLS data



# 5A beam line temperature (HLS)





# Vibration Measurement



# Measurement Sensor

## Electronics

Data Physics  
QUATTRO



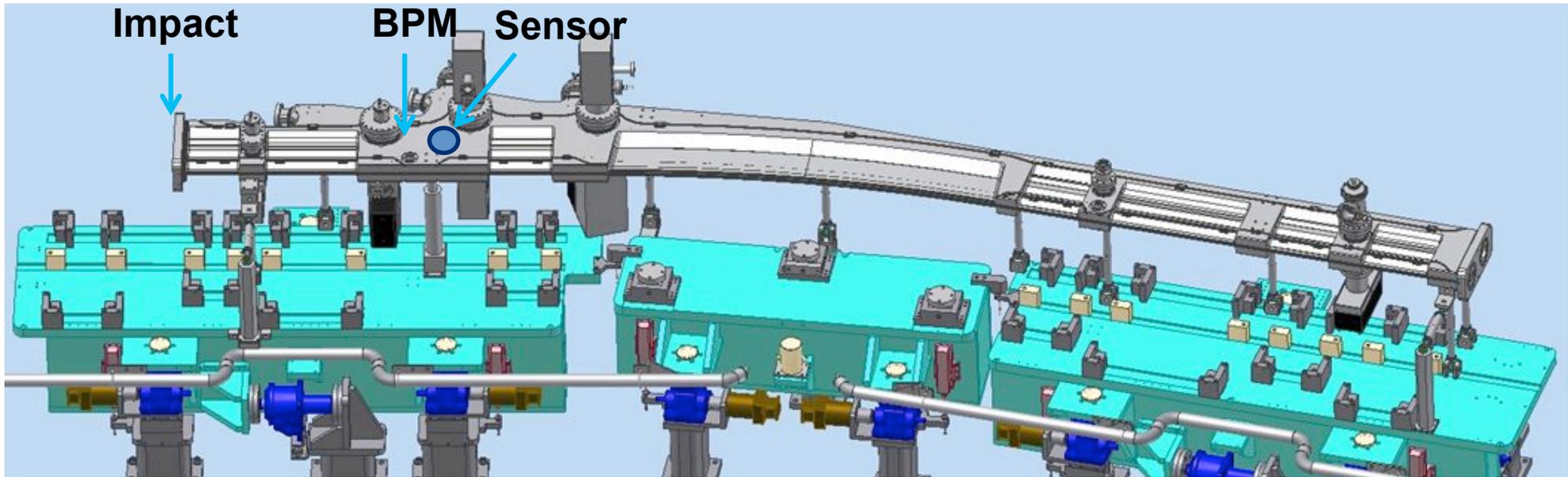
## Sensor

DYTRAN  
3191A  
SEISMIC ACCELEROMETER  
**SENSITIVITY 5 V/G**





# Natural frequency of a SR vacuum chamber

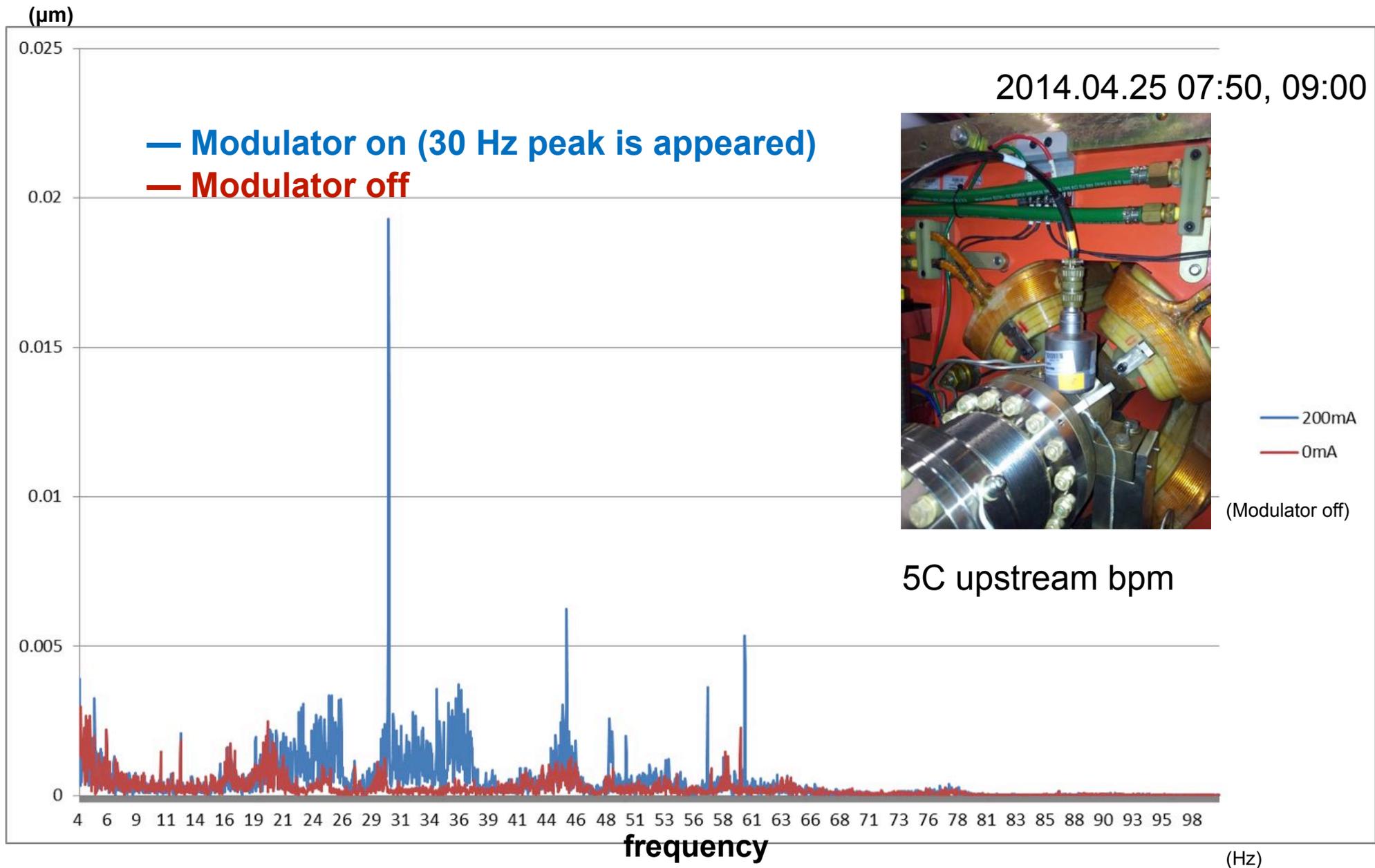


2014.04.09 10:30

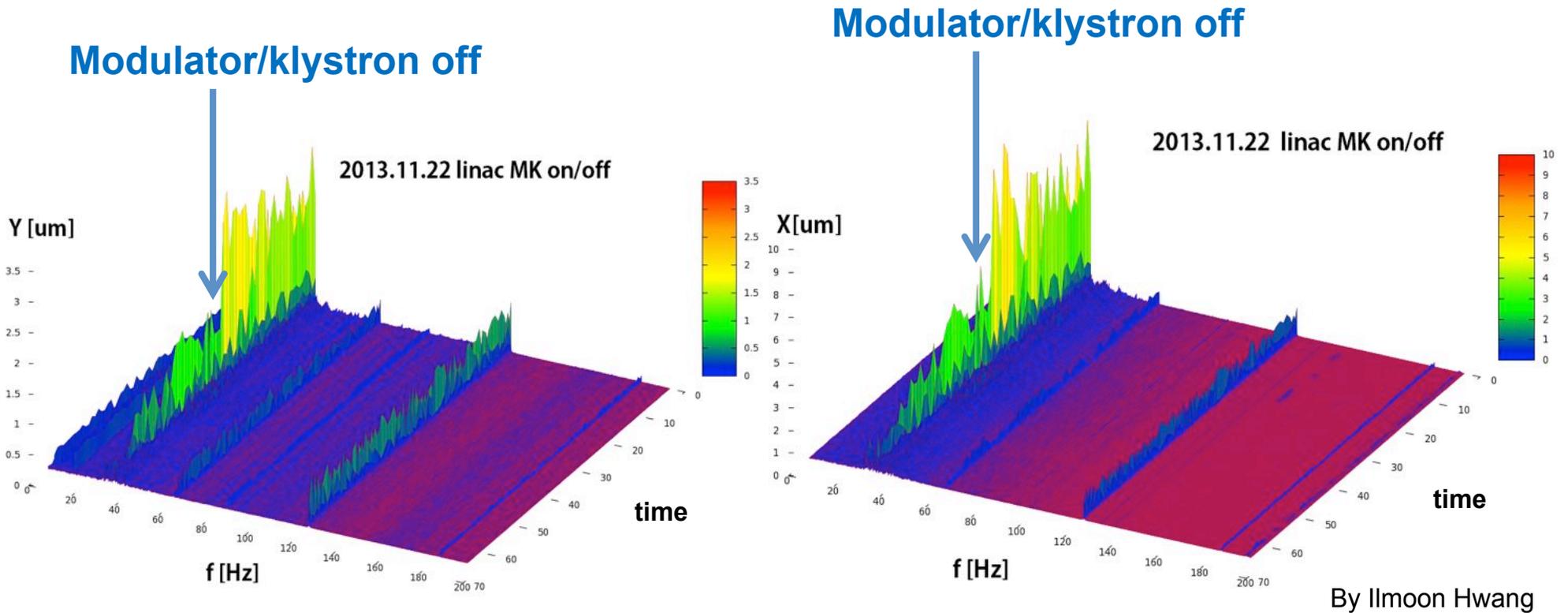


# Vibration due to Linac modulator/klystron

(Operation frequency of M/K is 30 Hz)



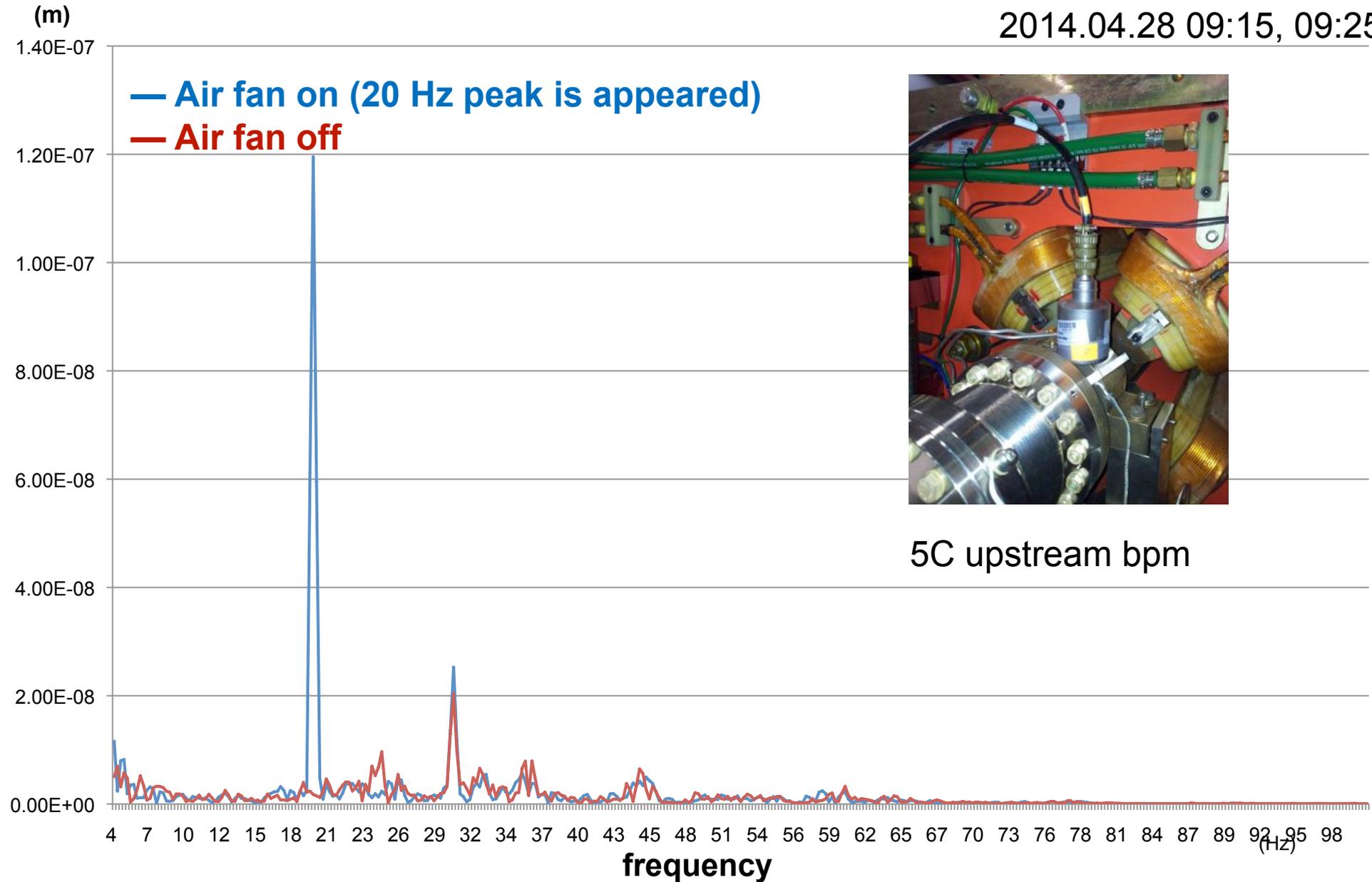
# Vibration monitored by electron BPM (Linac modulator/klystron on&off)



30 Hz vibration peak due to modulator/klystron is also appeared at electron BPM signal

# Vibration due to air fan of experimental hall

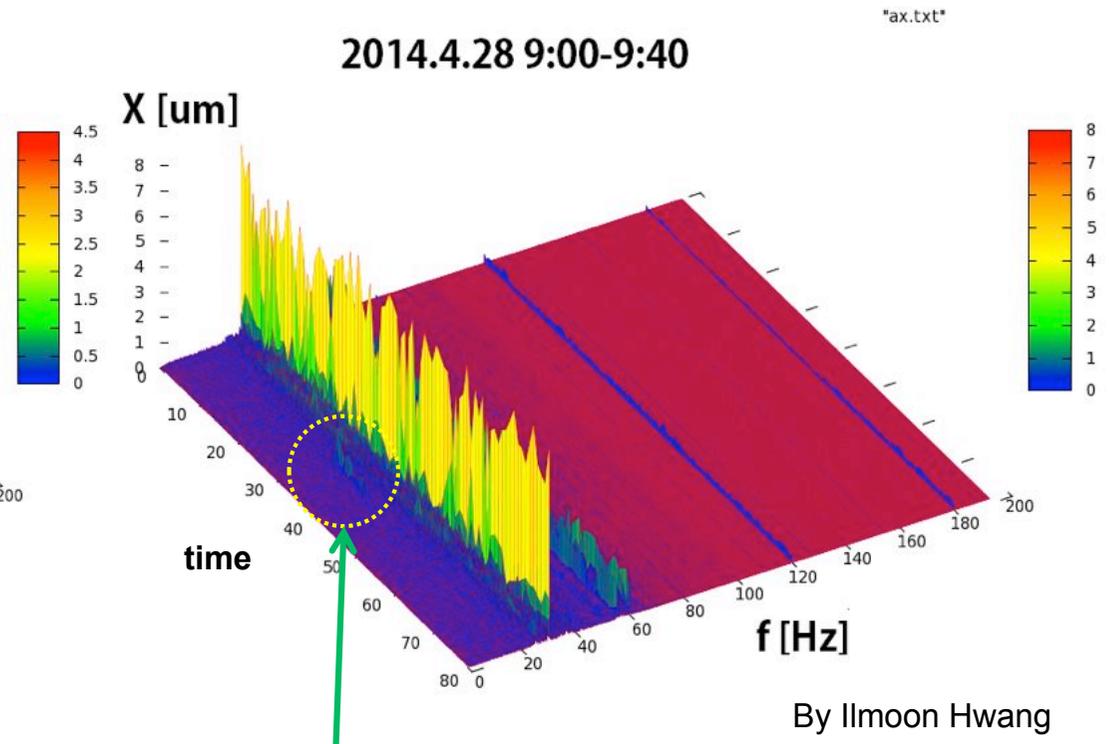
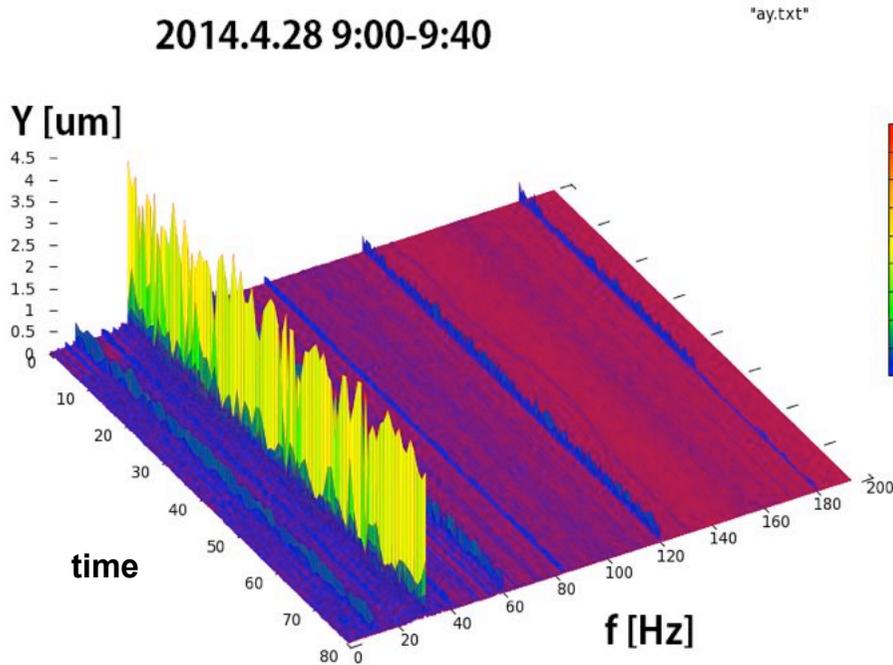
2014.04.28 09:15, 09:25



5C upstream bpm



# Vibration monitored by electron BPM (Air fan of experimental hall on&off)

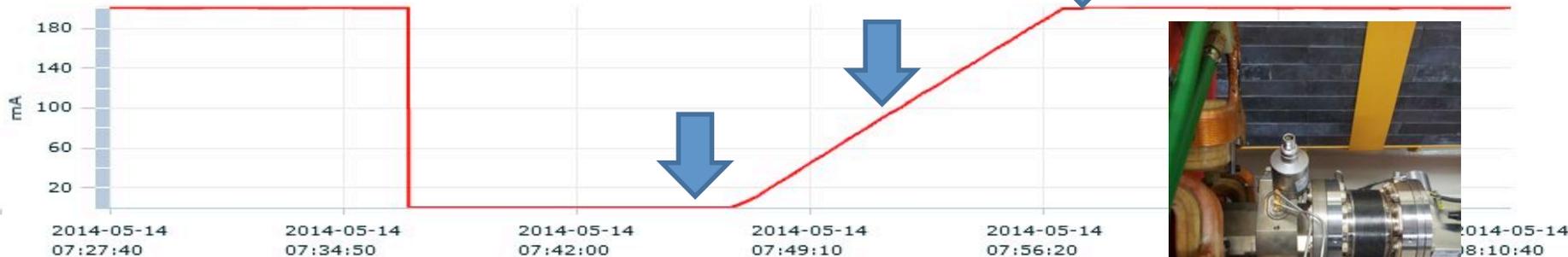


**Air fan on (20 Hz peak is appeared)**

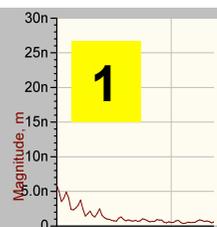
# Vibration during beam injection (10 Hz injection kicker)

SR:G00:BEAMCURRENT\_T

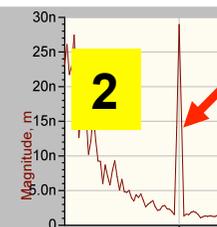
Max: 201.3350, Min: 9.3023, Avg: 130.3219, Last: 200.6950



5C downstream BPM

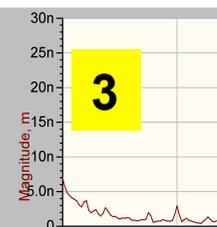


2014.05.14 07:45



10 Hz peak is appeared

2014.05.14 07:47



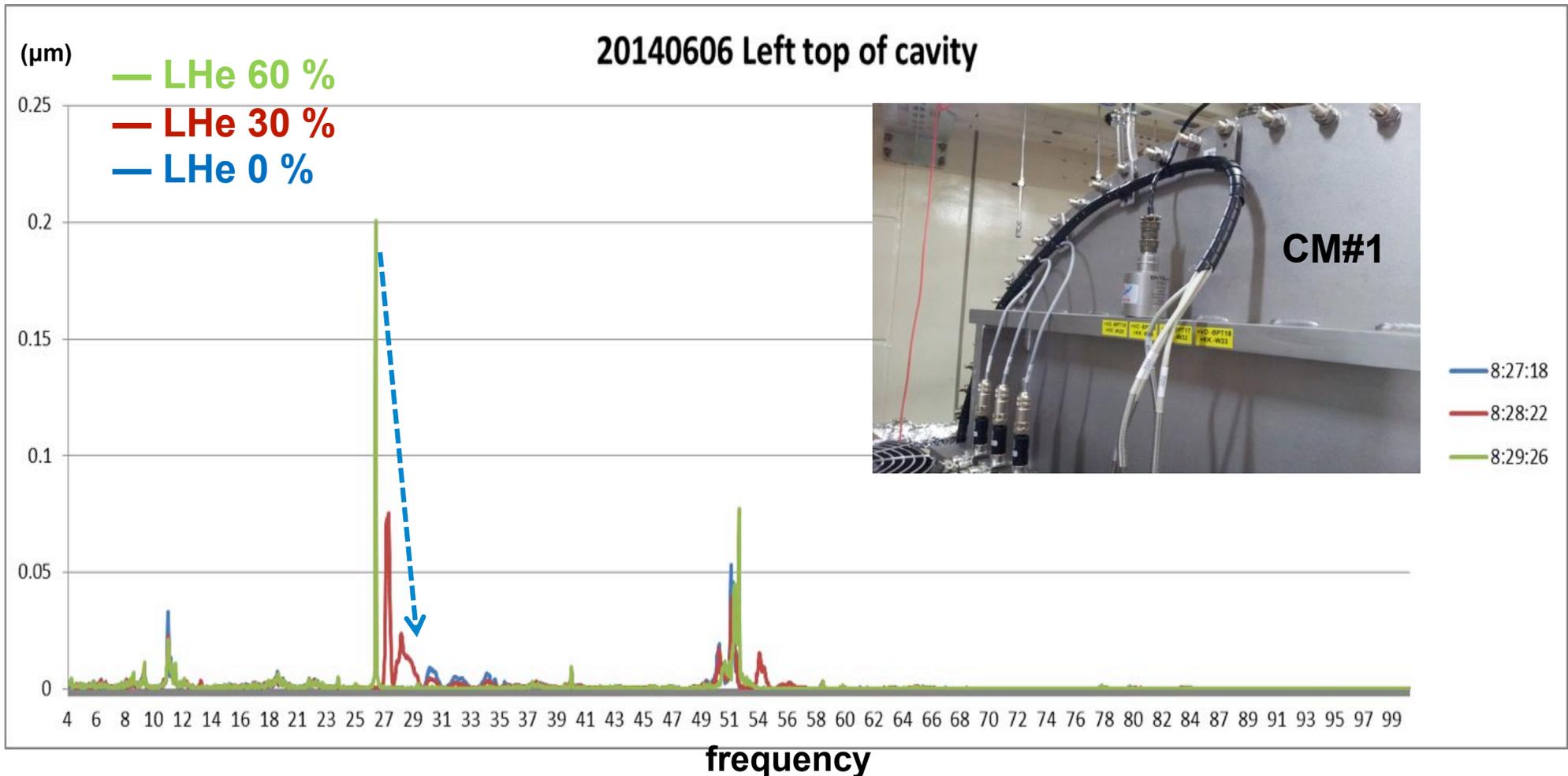
2014.05.14 07:58

frequency



# Vibration of super conducting RF cryo-module (during liquid He drain)

See next page





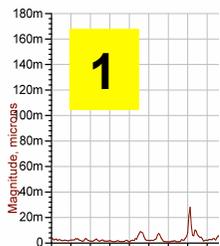
# Vibration of super conducting RF cryo-module (during liquid He drain)



26 Hz

G1, 1

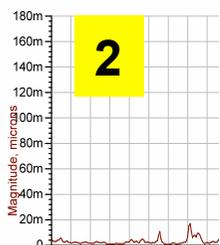
2014.06.27 10:22



G1, 1

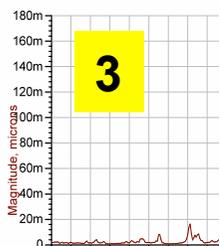
2014.06.27 12:00

Position and amplitude of vibration peak are changed according to LHe level



G1, 1

2014.06.27 13:00



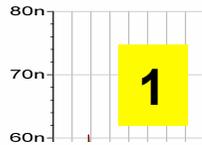
frequency



# Vibration of cooling water pipe attenuator

(before and after attenuator passage)

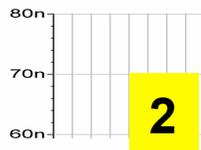
(m)



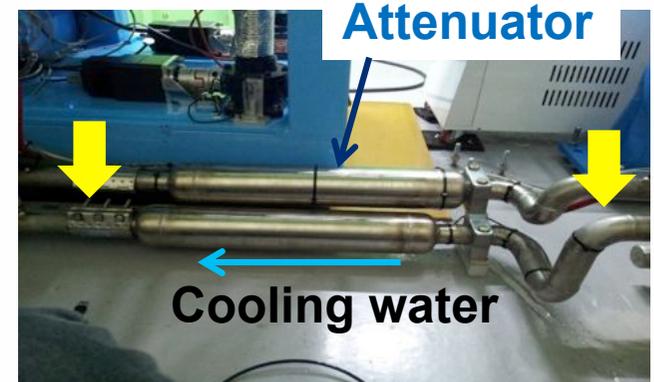
Before passing the attenuator

2014.05.16 02:30, 19:40

After passing the attenuator

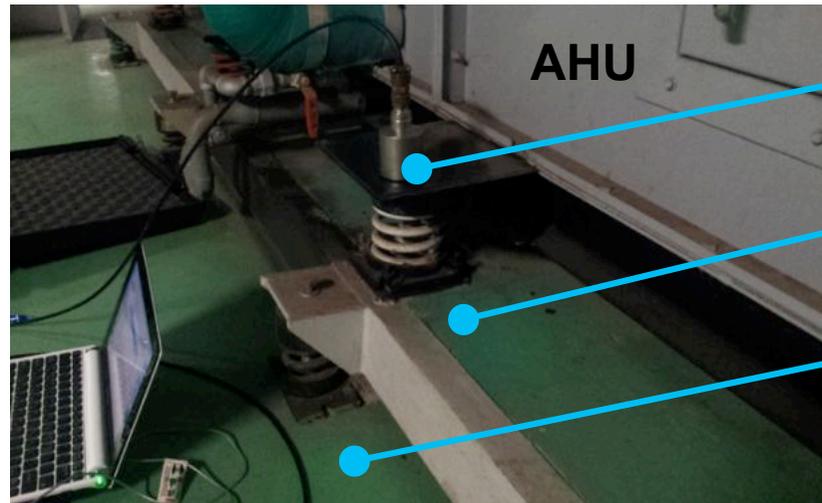


Frequency (Hz)



Frequency (Hz)

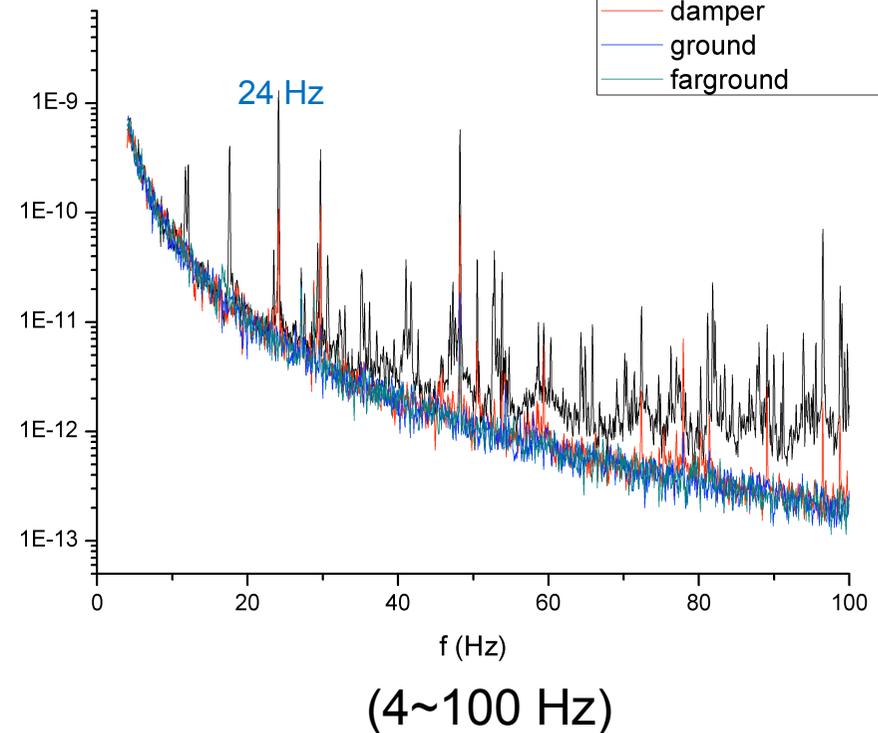
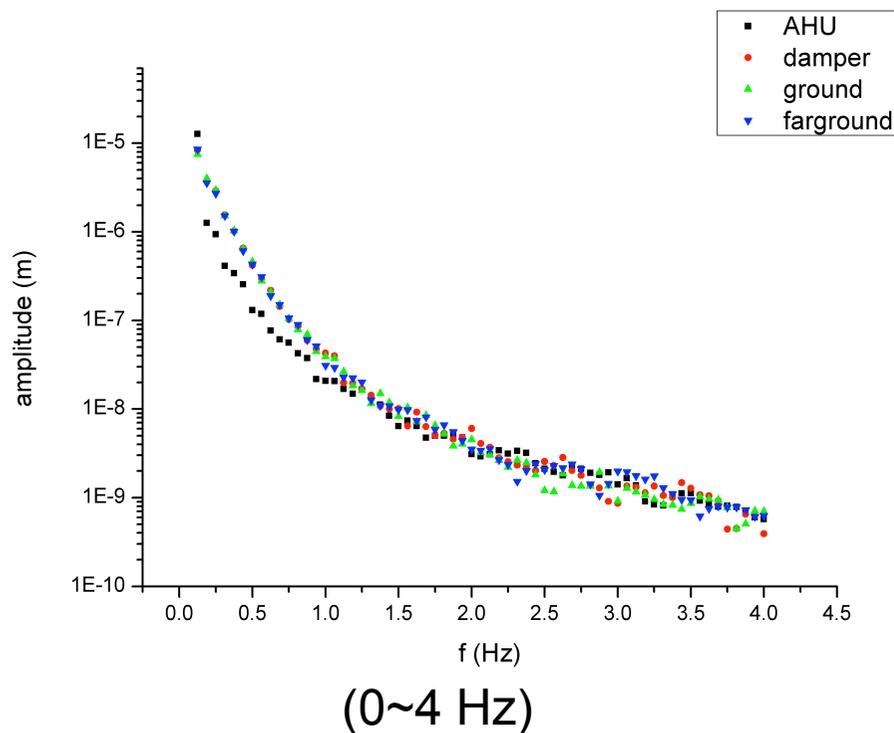
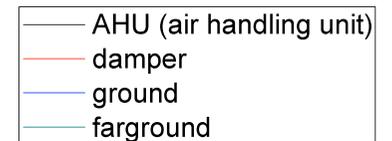
# Vibration due to Air Handling Unit (AHU)



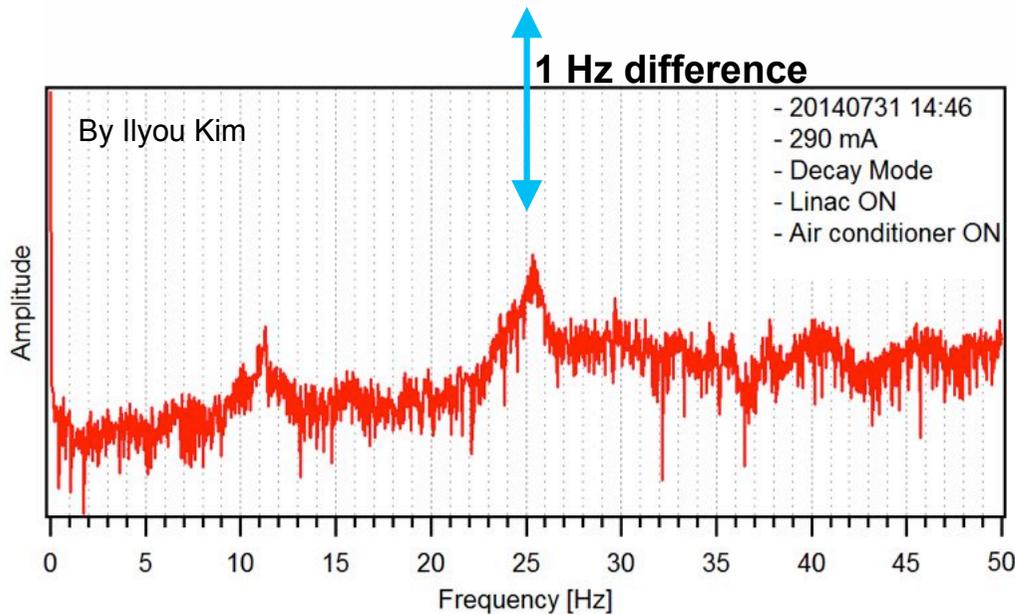
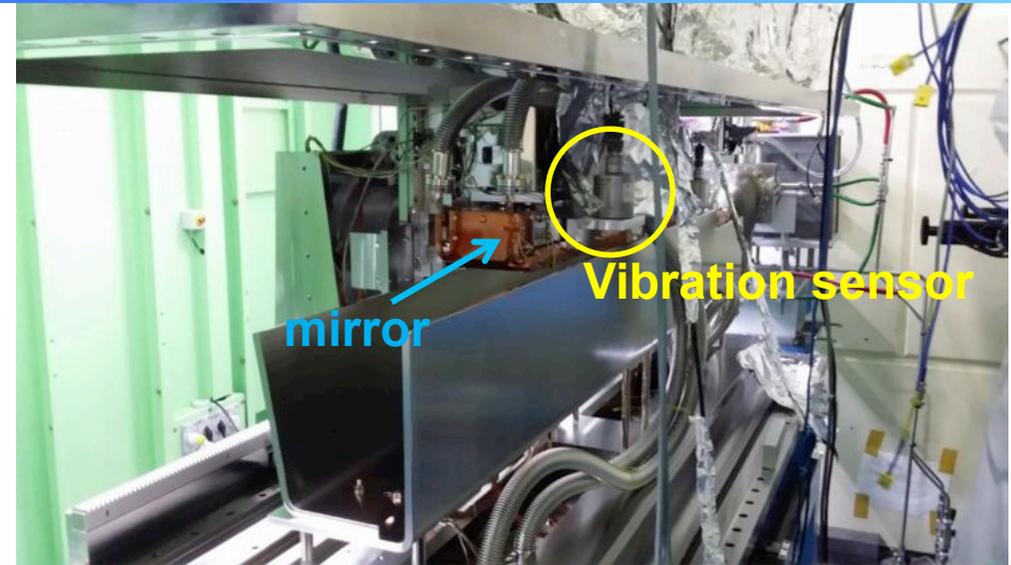
Vibration of AHU

Vibration at damper

Vibration at ground



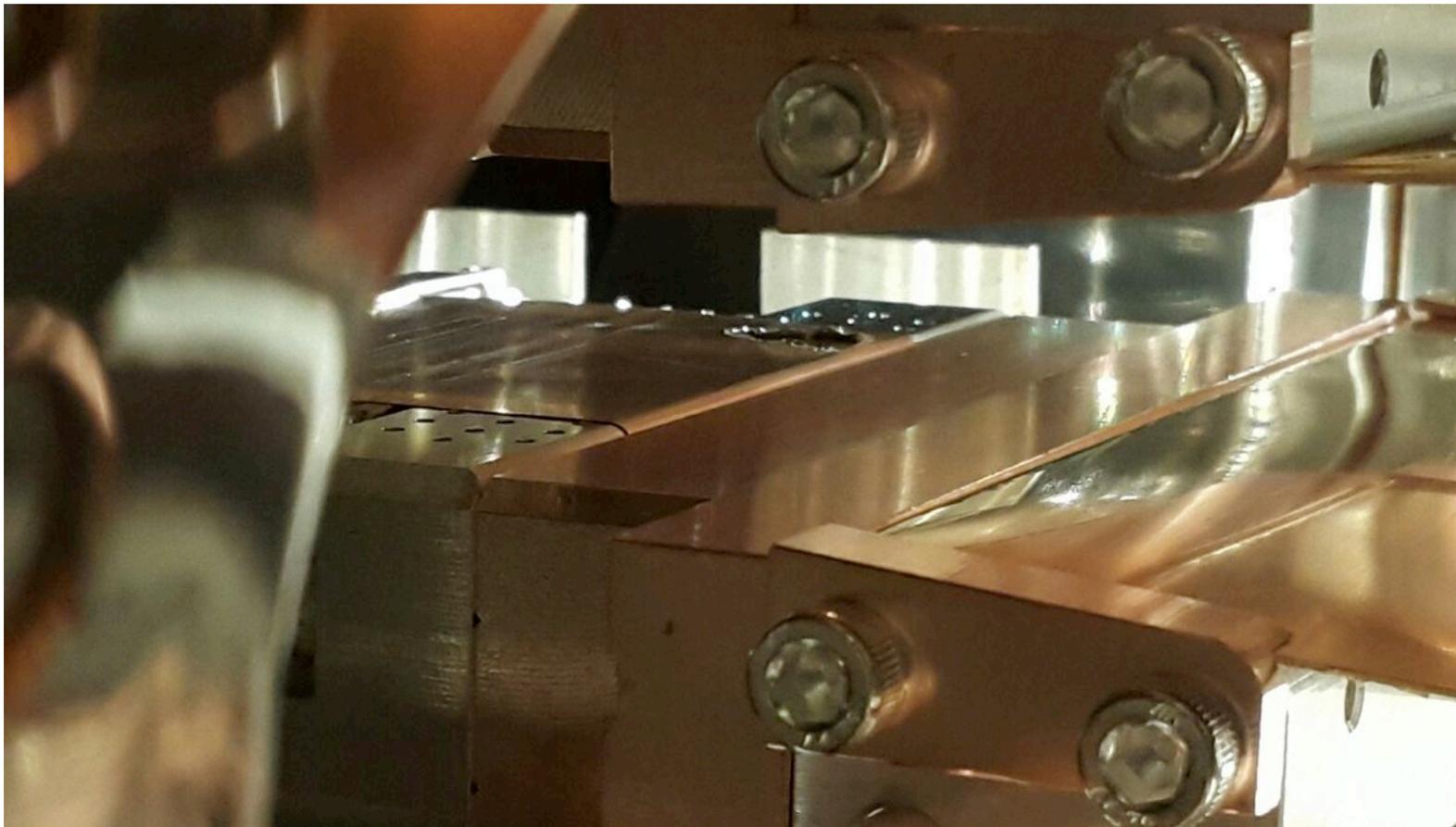
# Beamline image vibration vs. mirror

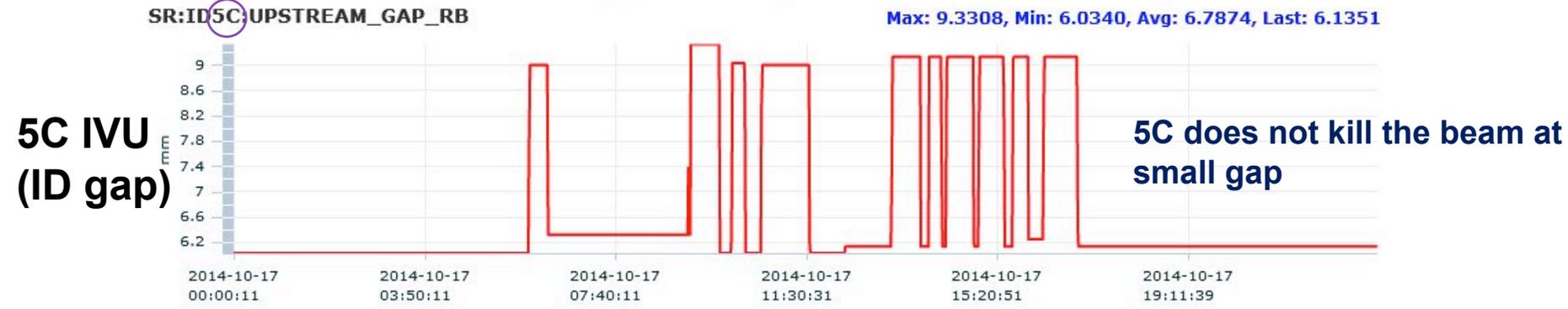
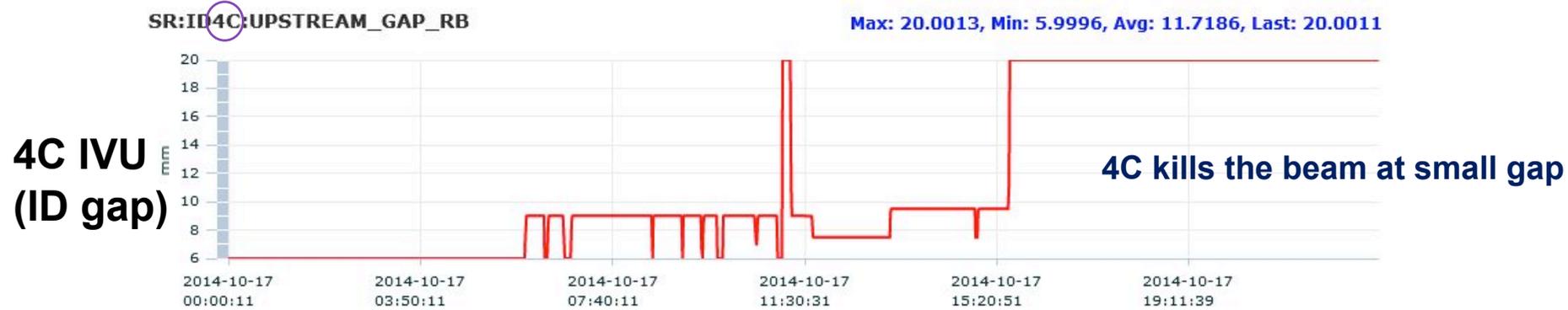


Frequency (Hz)

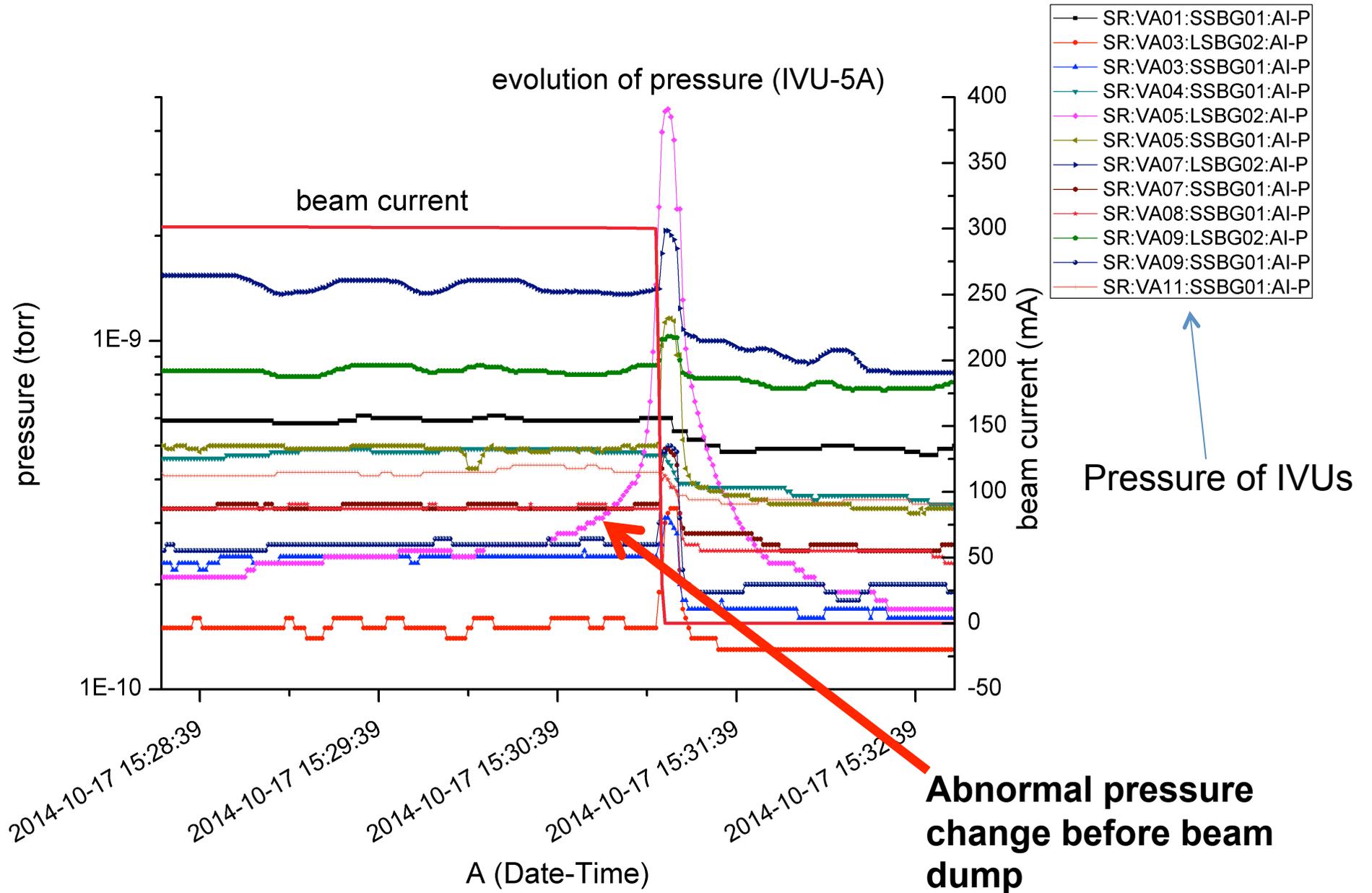
Frequency analysis from measured image data in 6C image beamline

# IVU foil bump

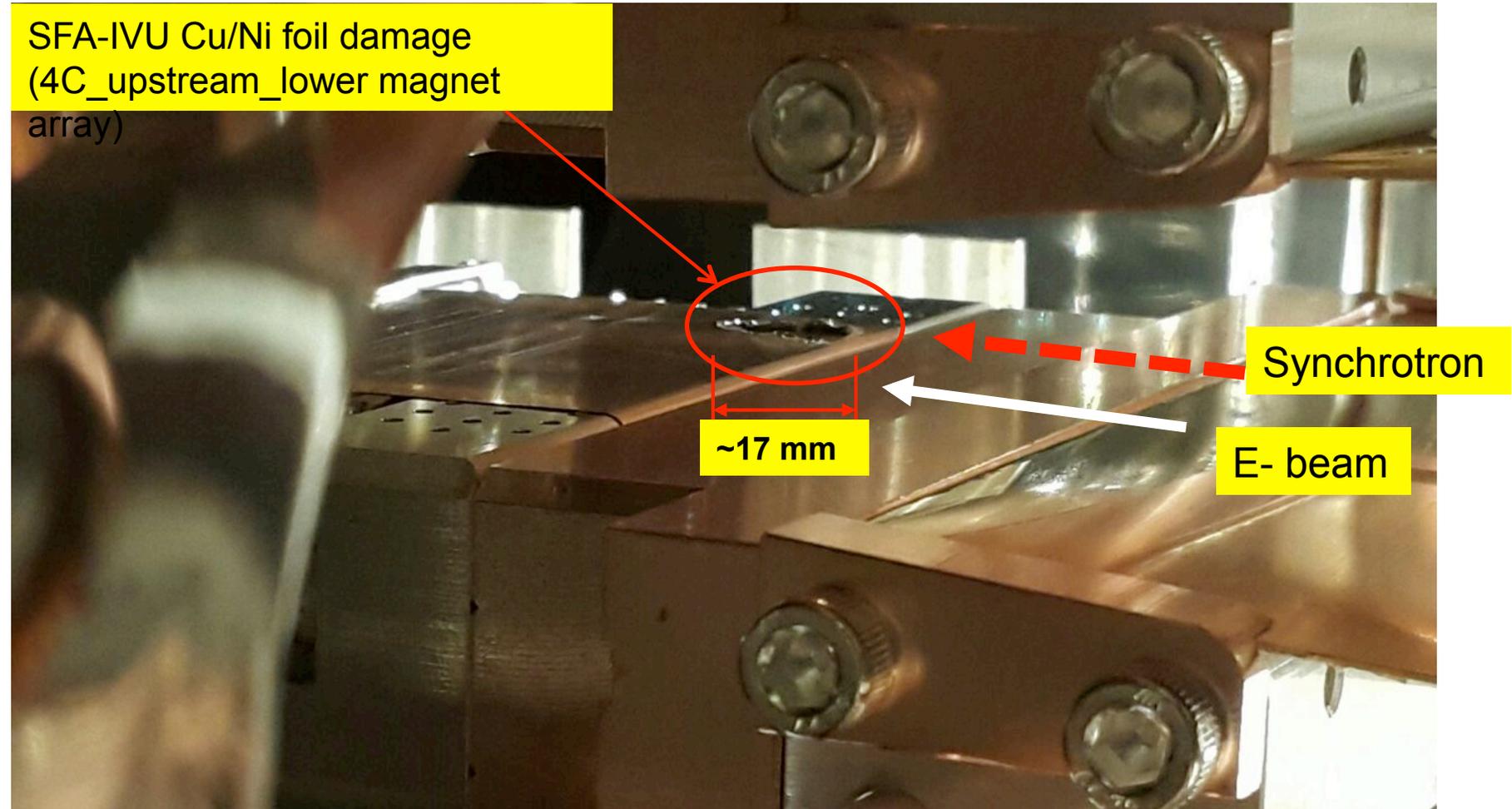




# Beam dump due to the IVU foil bump

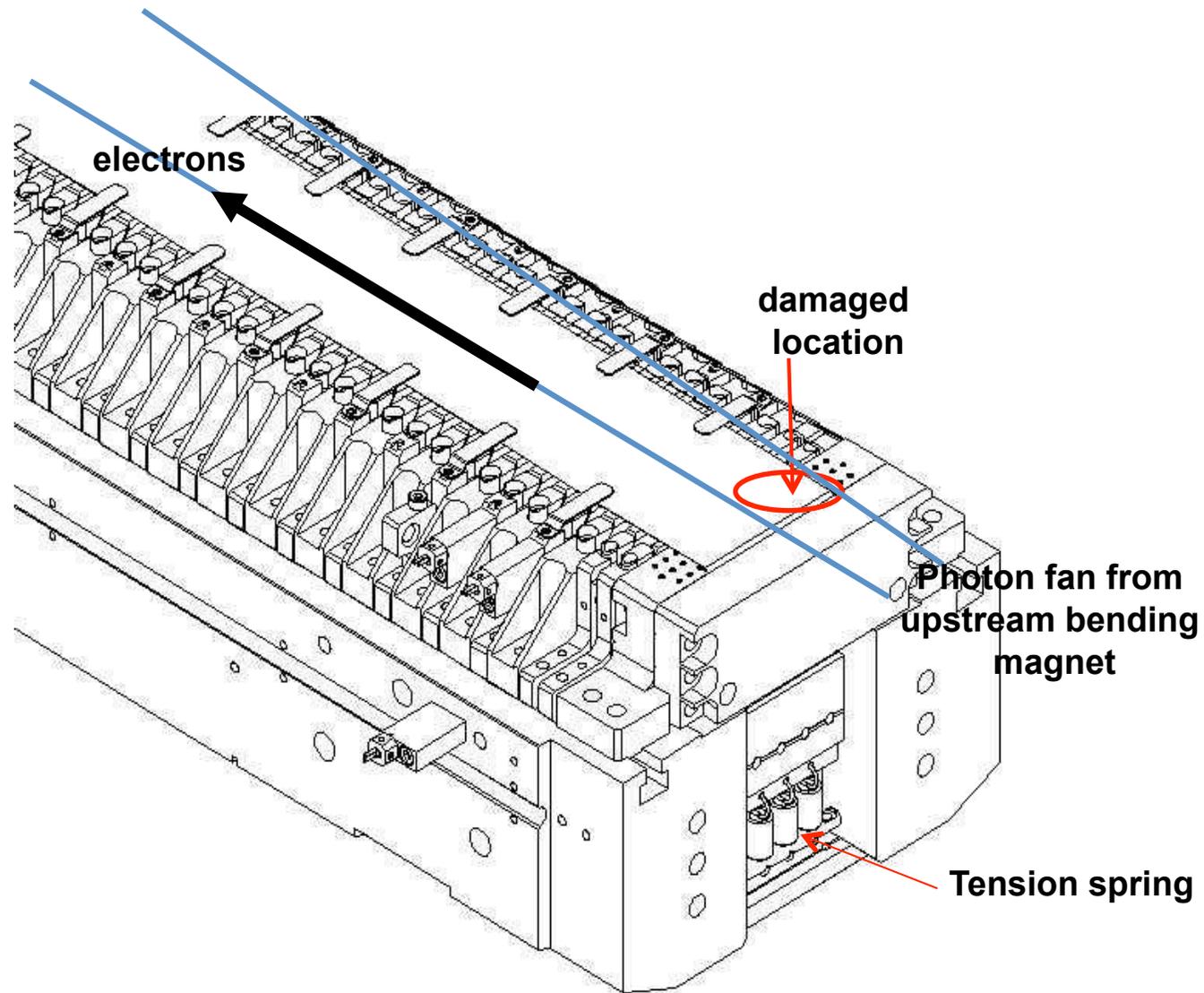


# Damaged IVU (4C)



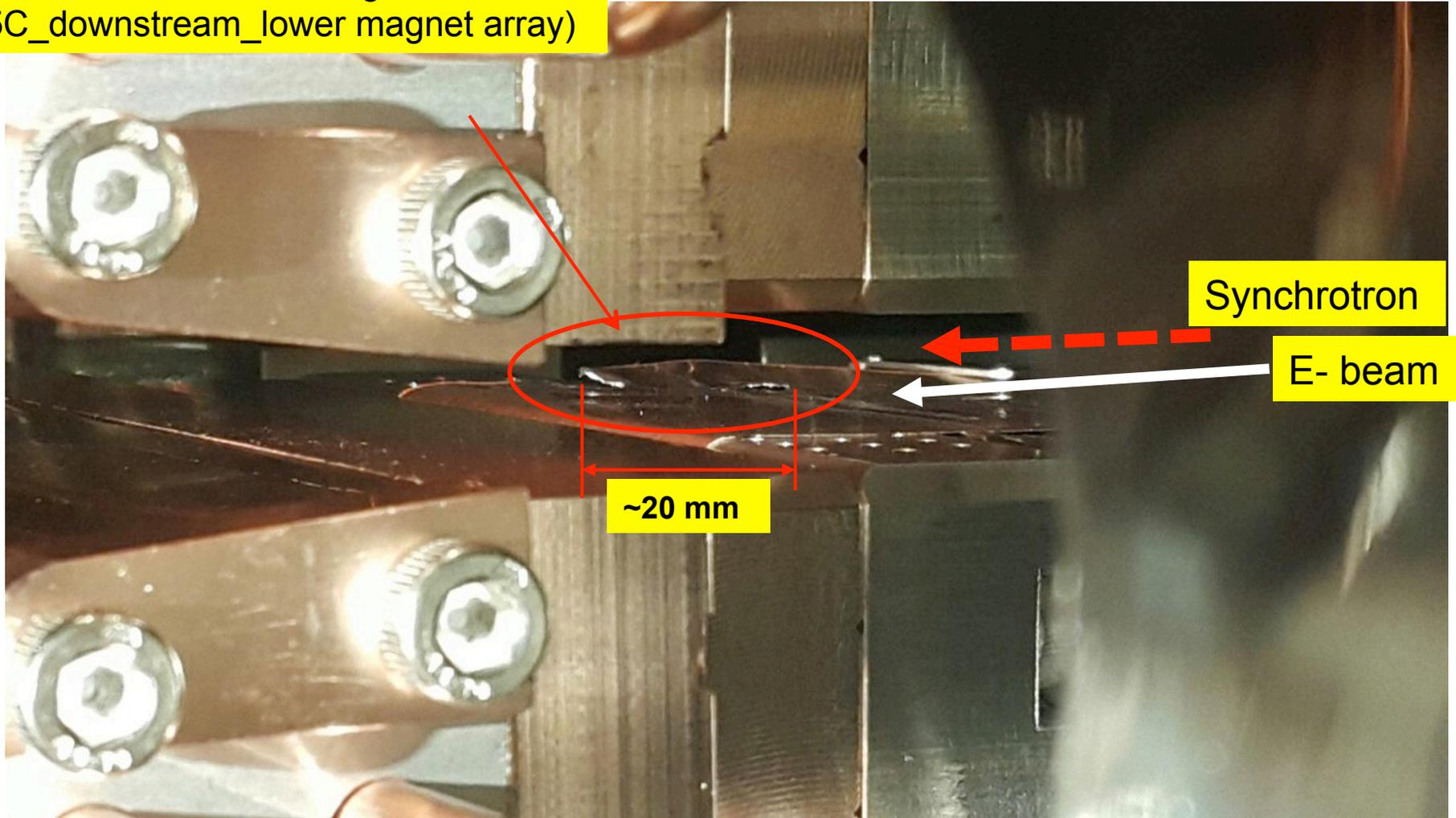
1. foil bump → image current heating → bump height ↑ → synchrotron heating → foil melting (1,2,3 호기)
2. foil bump → image current heating → bump height ↑ → Beam mis-steering (including mis-alignment) (lower foil only + cell 4,5)

SFA-IVU Cu/Ni foil damage  
(4C\_upstream\_lower magnet array)



# Damaged IVU (5C)

SFA-IVU Co/Ni foil damage  
(5C\_downstream\_lower magnet array)

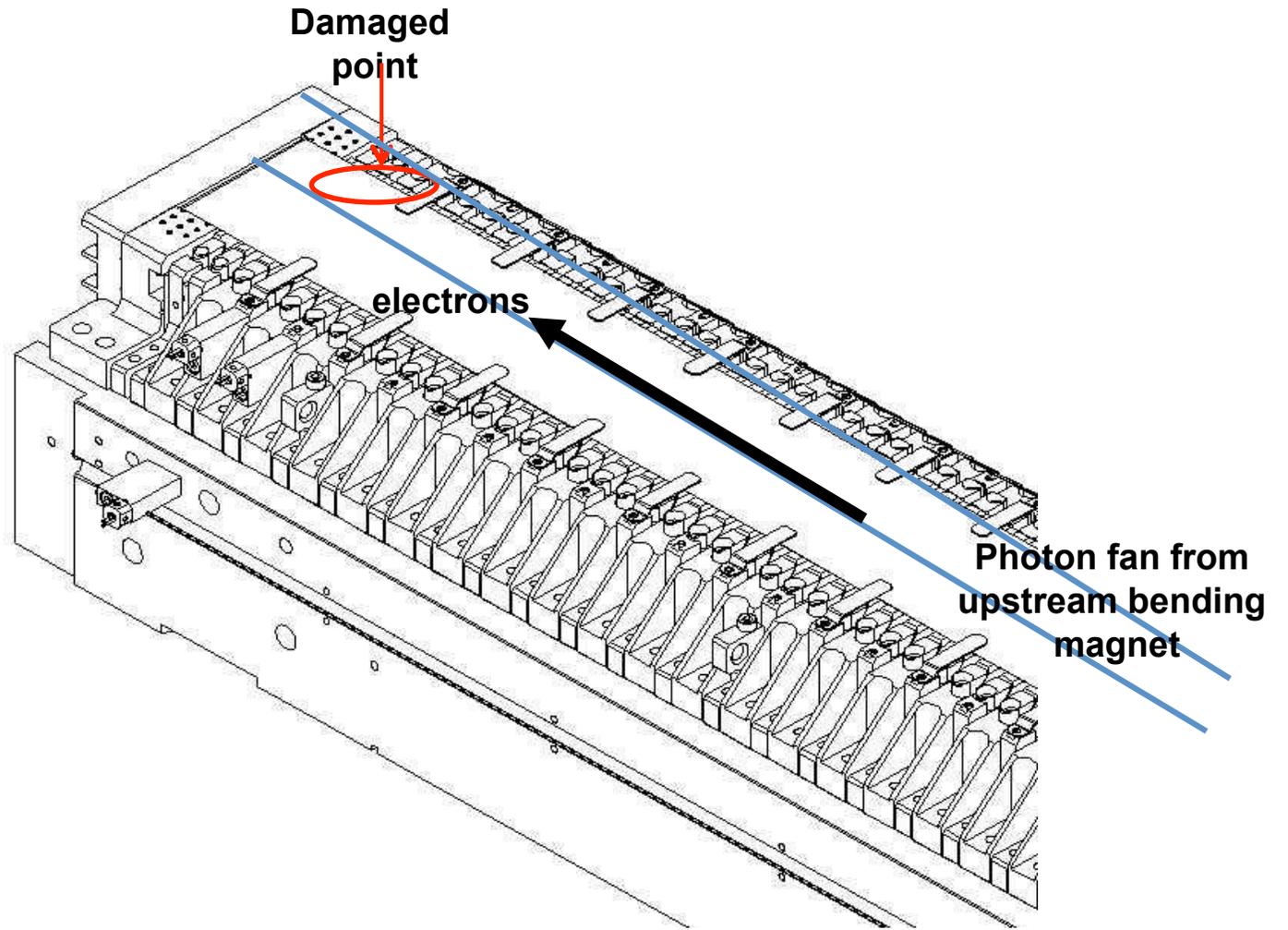


Synchrotron

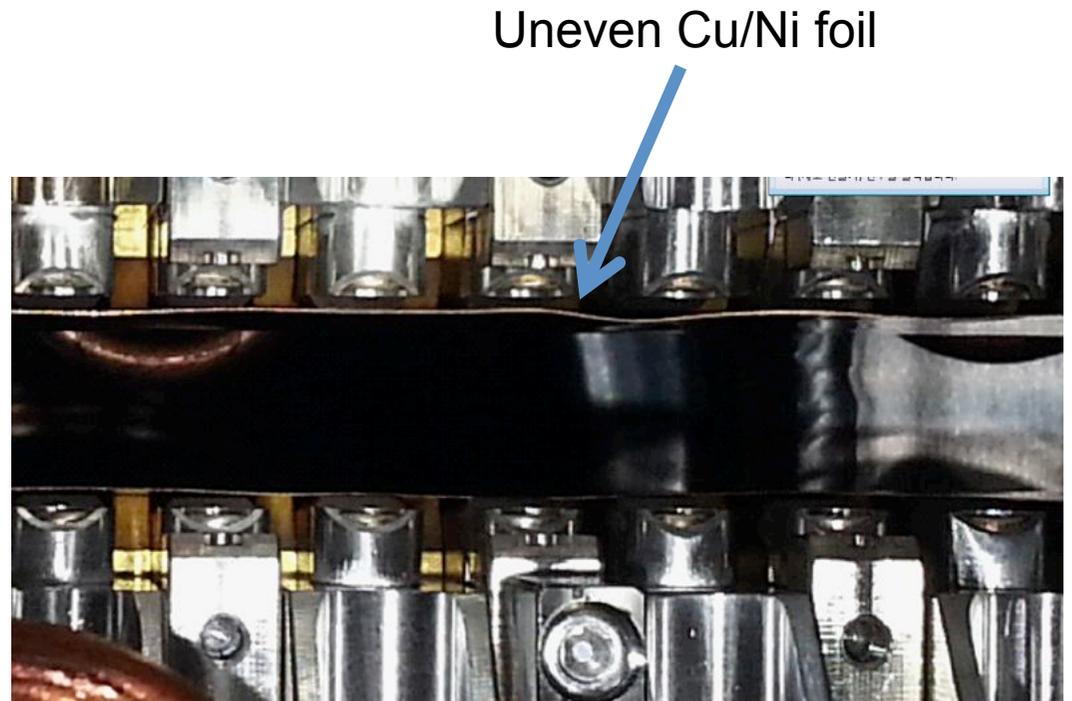
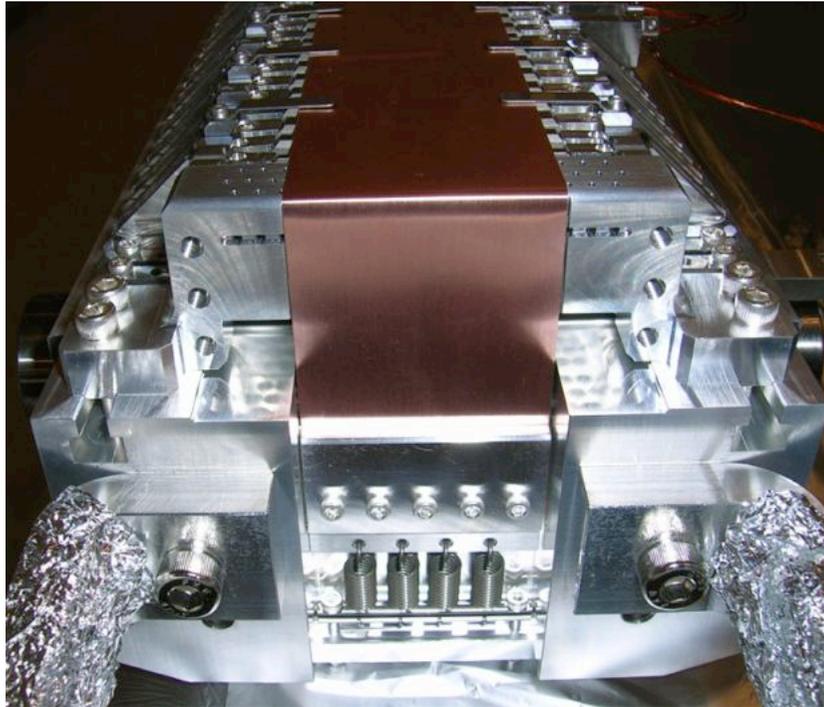
E- beam

~20 mm

SFA-IVU Cu/Ni foil damage  
(5C\_downstream\_lower magnet array)



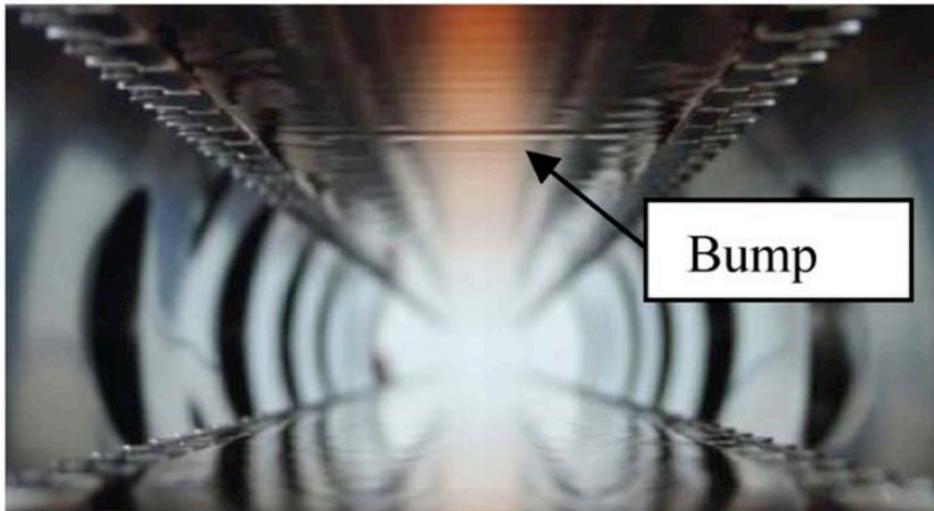
# Inside of the IVU20



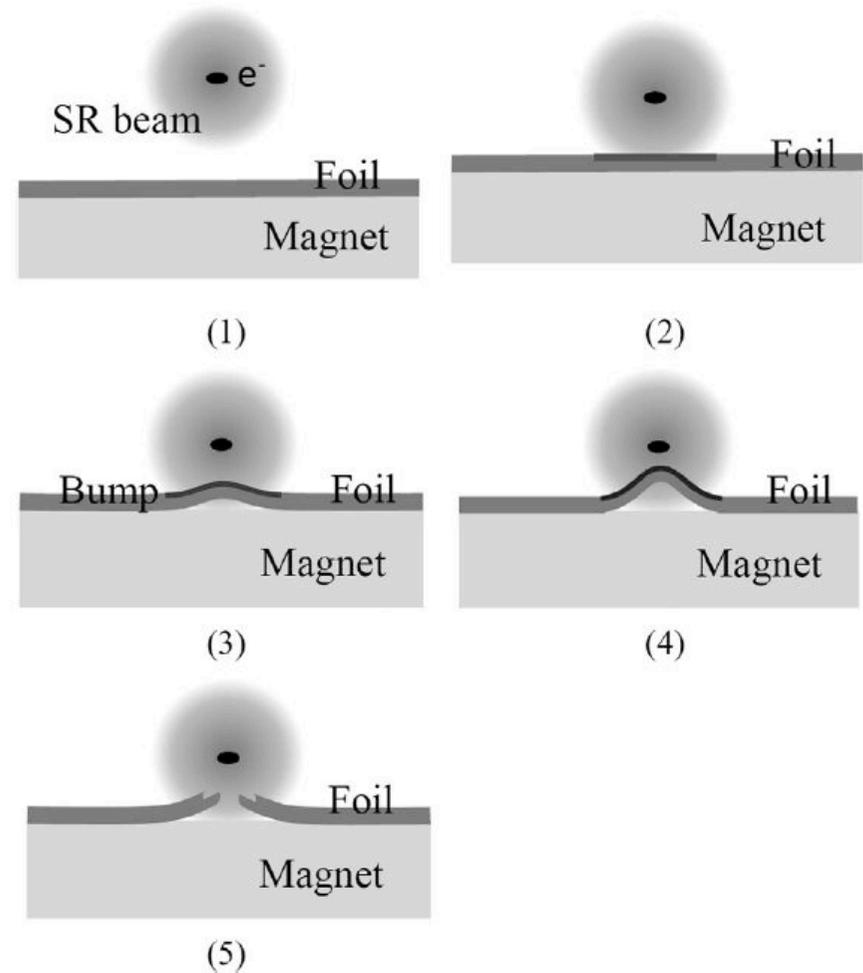
Side view

(Picture taken before assembling)

# IVU trouble in NSRRC



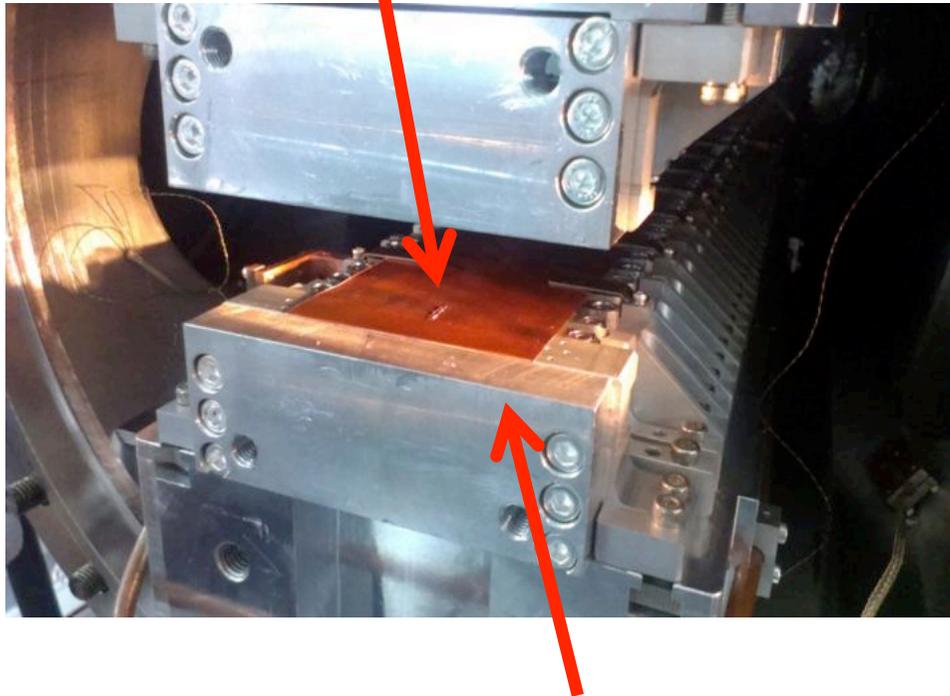
Bump on the magnet foil after baking  
(Before operation)



Scenario of an avalanche meltdown  
due to a beam-induced heat load

# IVU trouble in SSRF

Because the copper foil drum up,  
this scratch may be cut by beam



Reinstalled the block to make the copper  
foil smooth

# Repair status

- Cu/Ni foil (50 um/50 um thickness) has been arrived from NSRRC.
- IVU20(4C) in the SR tunnel was replaced with pre-ID chamber.
- IVU20(4C) has been moved to Support Bldg.#2 for repair. (2015.01)
- IVU20(4C) will be reinstalled in 2015.08 (summer shutdown)



Storage Ring Tunnel

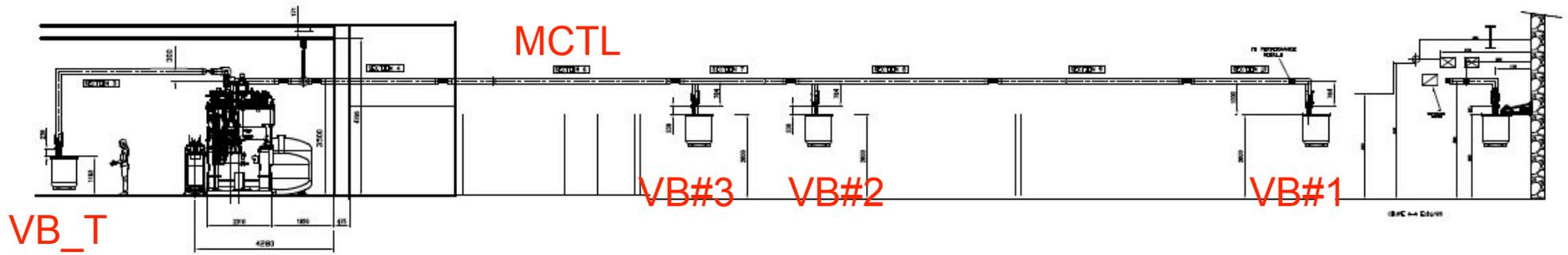
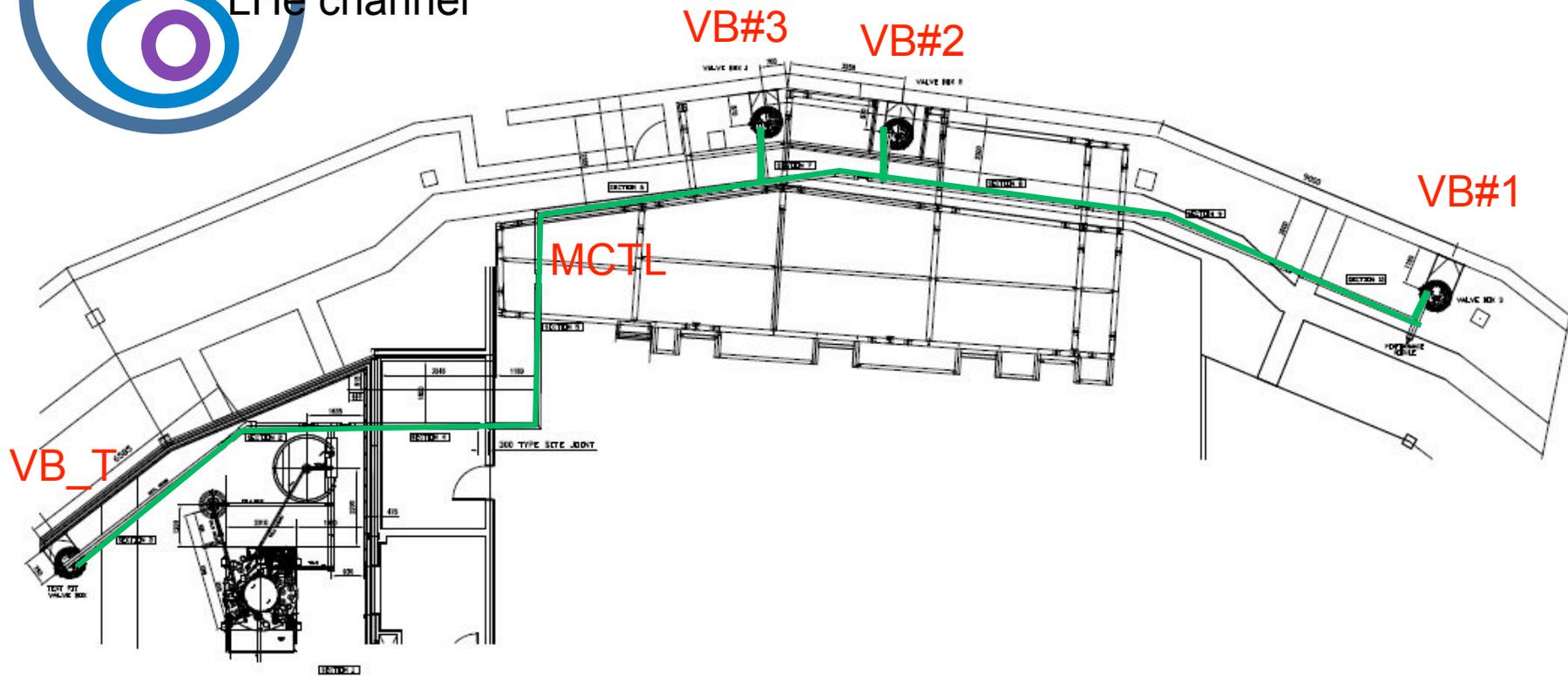
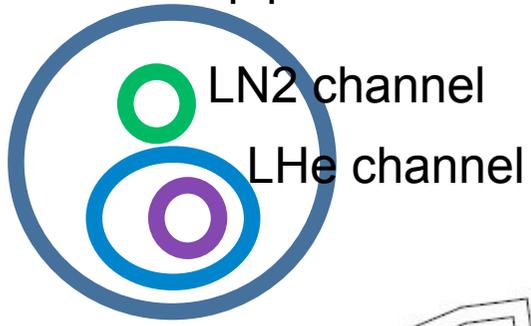


Support Bldg. #2

# MCTL break down

Vacuum pipe

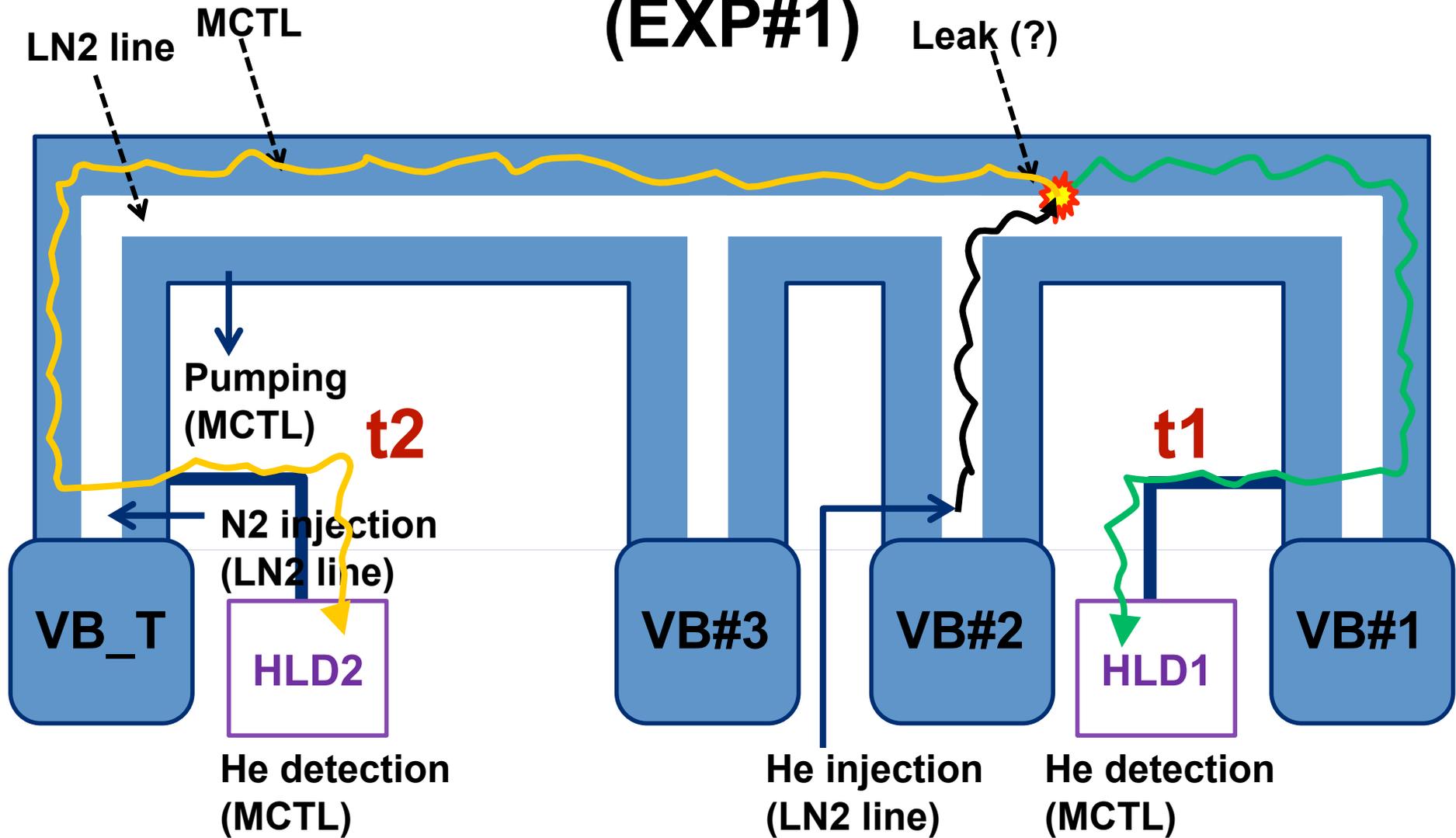
# MCTL layout



# Leak Detecting Procedure

1. Place two He leak detectors(HLDs) on the LN2 line and inject He gas into MCTL pipe or vice versa.
2. Check the He detecting time between two HLDs.
3. The leakage is nearer to the HLD which detects He first. (If the pressure in the LN2 pipe is uniform, then the He diffusion velocities are equivalent)
4. If the time difference is negligible, inject little amount of N2 gas into the LN2 line to increase the He diffusion time in the line. Then check the time difference again.
5. Change the N2 background pressure in the LN2 line to confirm the He arrival time delay.
6. If the pressure of LN2 line is too high then we have severe pressure gradient in the pipe (because two HLDs are pumping at different places). In this condition the He diffusion velocity is not uniform. This causes an error.

# (EXP#1)

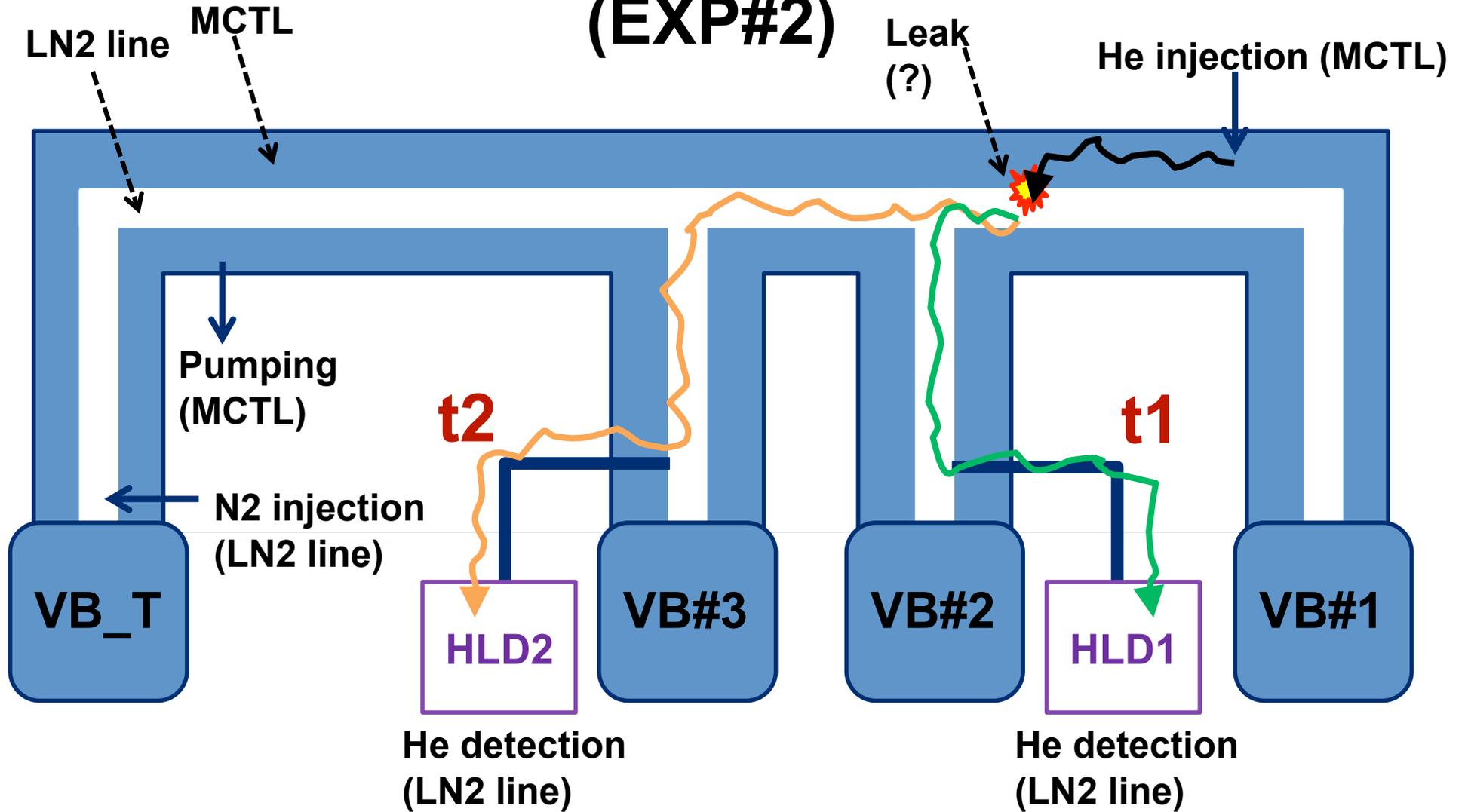


P (LN2 line)	t1	t2
< 0.01 mbar	72 sec	88 sec

→ Leakage is nearer to VB#1 than VB\_T

- HLD: He detector
- VB: Valve box

# (EXP#2)

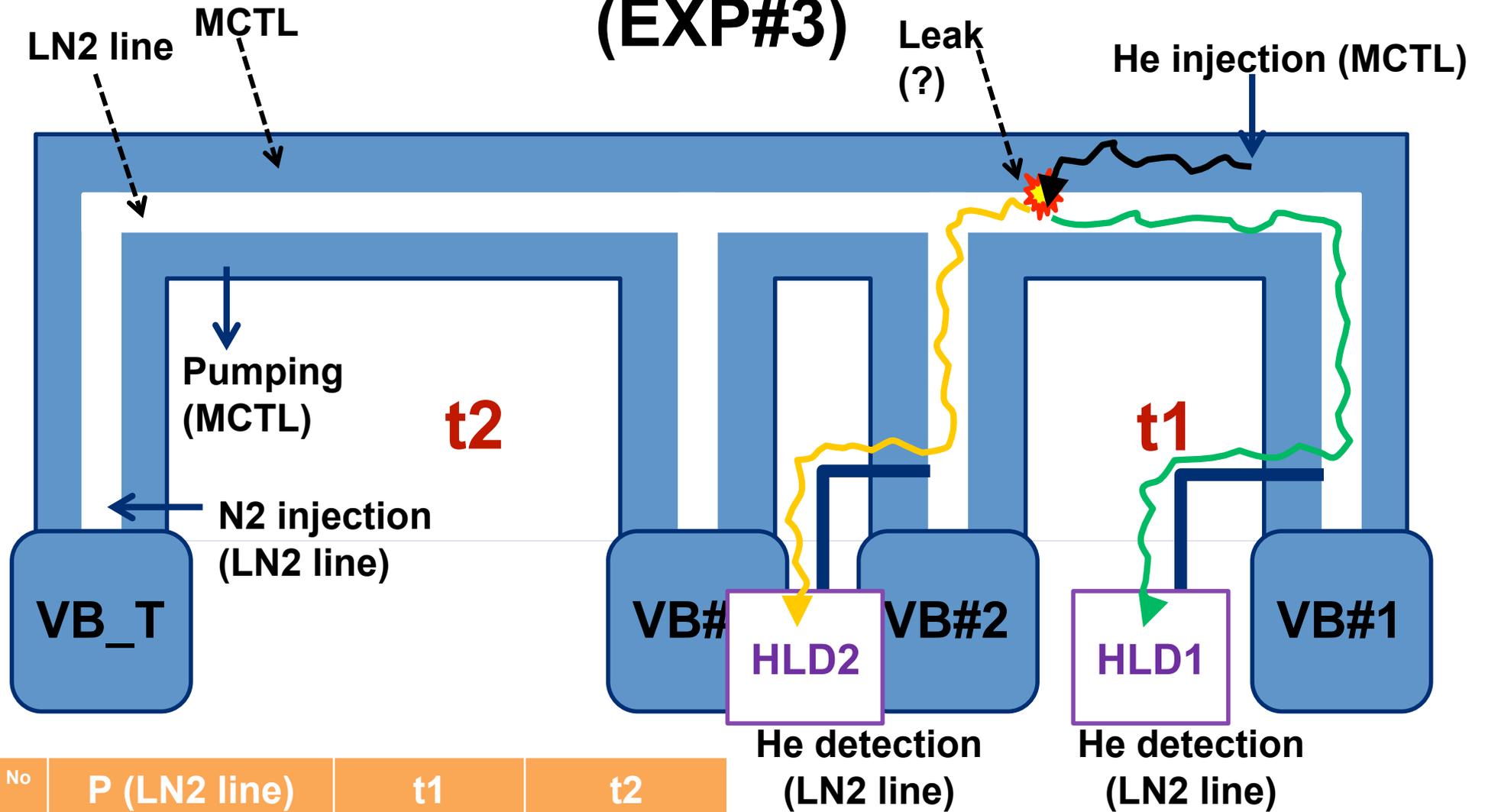


No	P (LN2 line)	t1	t2
1	< 0.01 mbar	16 sec	16 sec
2	< 0.05 mbar	12 sec	20 sec
3	< 0.1 mbar	13 sec	35 sec

→ Leakage is nearer to VB#2 than VB\_#3

- HLD: He detector
- VB: Valve box

# (EXP#3)



No	P (LN2 line)	t1	t2
1	< 0.01 mbar	8 sec	4 sec
2	< 0.02 mbar	18 sec	7 sec
3	< 0.05 mbar	26 sec	12 sec
4	atm (MCTL vented)	9 m 12 s	9 m 25 s

→ Leakage is nearer to VB#2 than VB\_#1

- HLD: He detector
- VB: Valve box

# Damaged bellows



Bellows @ Section 8



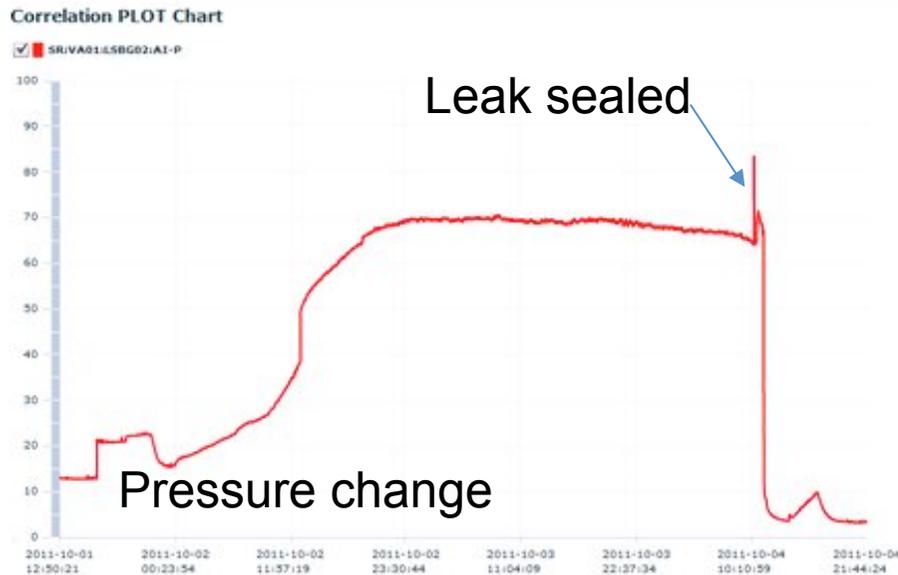
LN2 line spacer must be at upstream of LN2 flow, but it is at downstream.

# **Other vacuum related events during PL S-II operation**

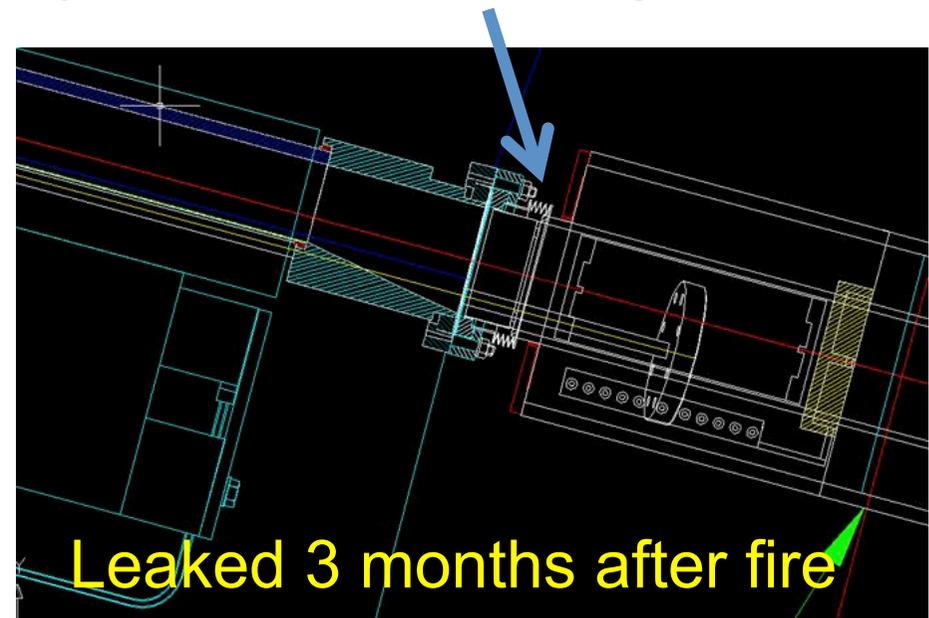
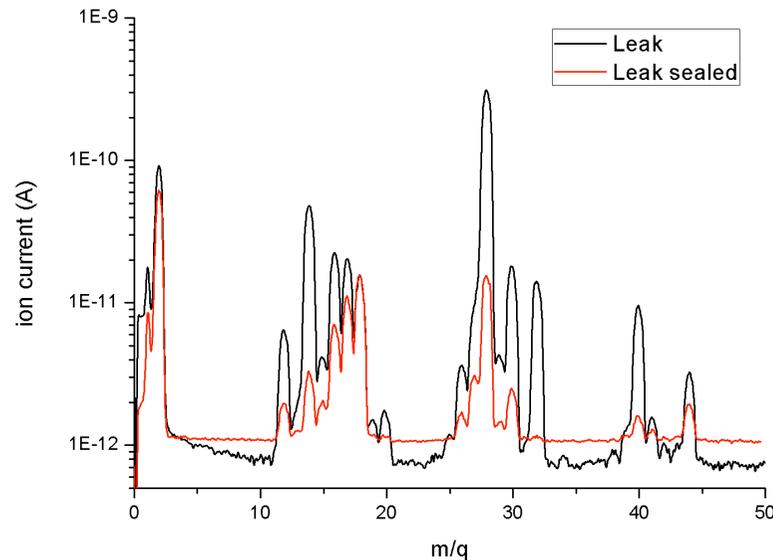


# Leakage in injection section (after fire)

(2011.10)

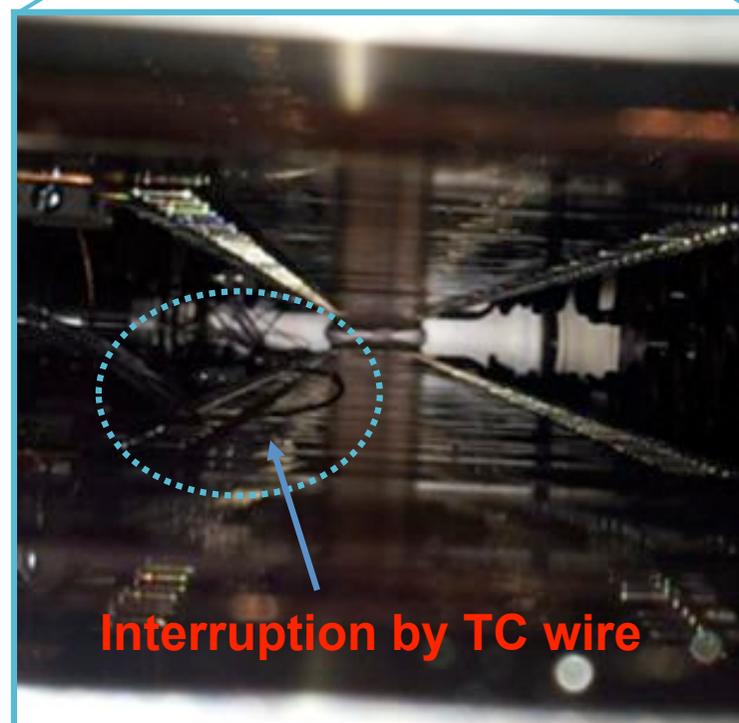
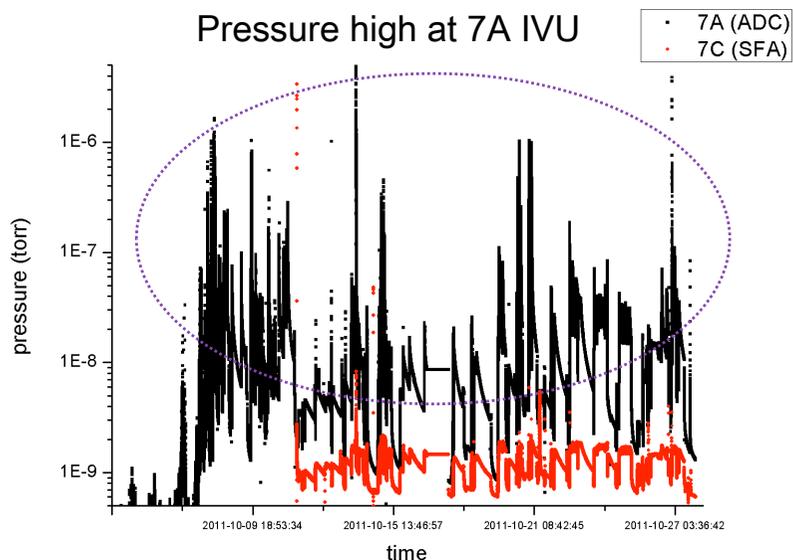
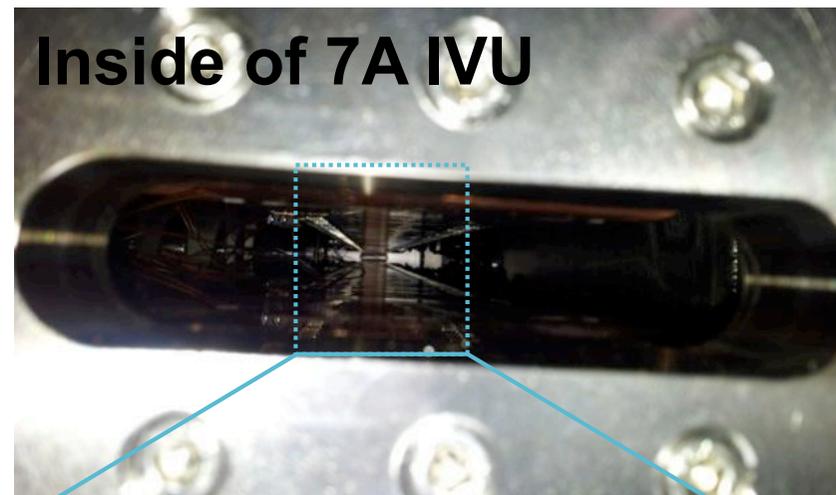
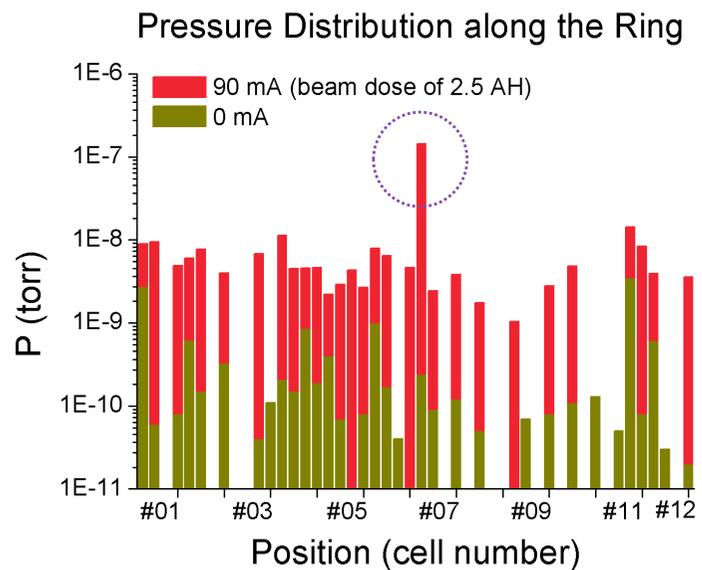


Weld joint of bellows was corroded by particles produced during fire



# Abnormal pressure in an IVU

(2011.10)



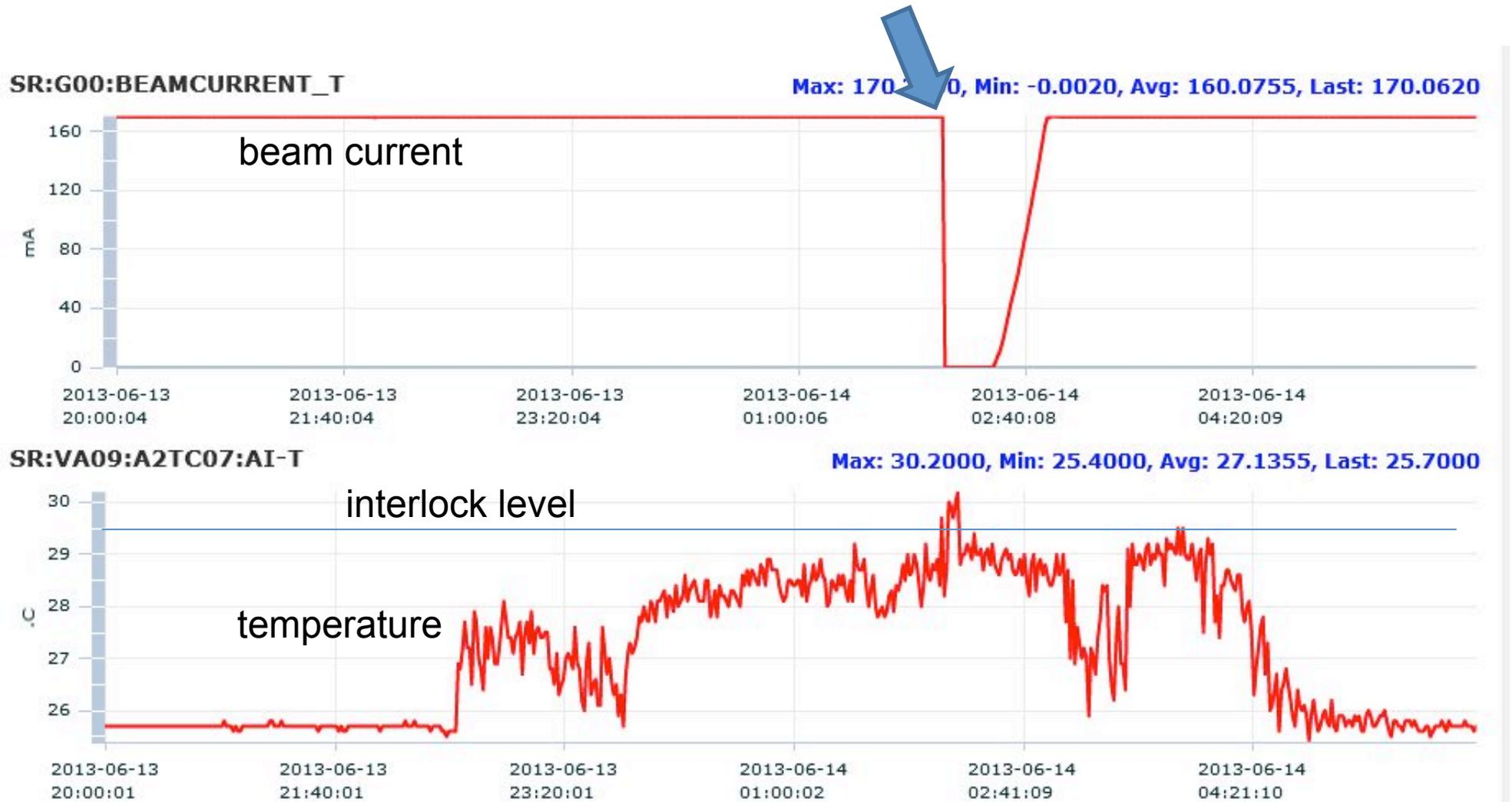
→ Changed with the spare IVU



# Thermocouple malfunction

(2013.06)

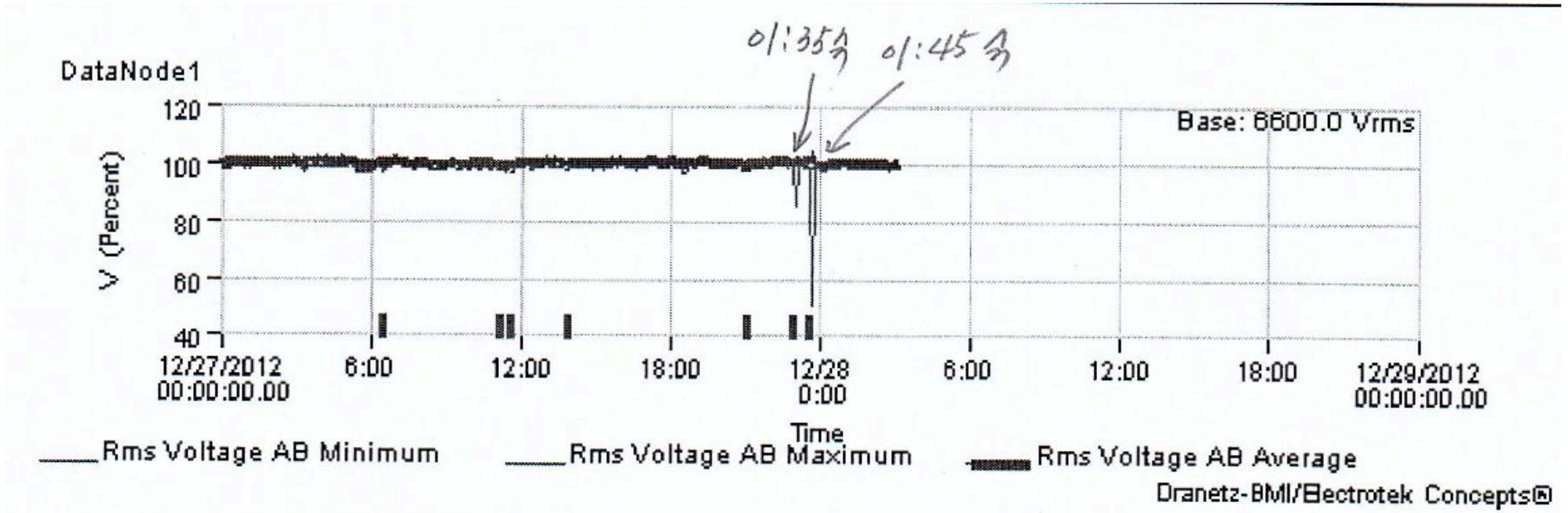
Beam was dumped due to the malfunction of a thermocouple out of 720 ea



Any recommendation to prevent this?



# Gauge controller malfunction due to sag



Old Ion gauge controller (GP307)

Instantaneous voltage sag → gauge controller emission off →

Analog output sent 10 V signal → Machine Interlock System triggered

→ Gate valve closed → beam dump

(The controller being in trouble was changed then it became O.K.)

Thank you for your attention!

